TOLT RIVER WATERSHED ANALYSIS SURFACE EROSION ASSESSMENT MODULE _ROADS_

The following report summarizes the results of the road surface crosson assessment module conducted for the Tolt River watershed. All products, including forms and maps, have been reviewed by the Tolt Watershed Analysis participants and their comments have been incorporated.

Prepared for Weyerhaeuser Company

In accordance with Standard Methodology for Conducting Watershed Analysis Chapter 222-22 WAC, Version 1.P

Washington Forest Practices Act Board Manual

TOLT WATERSHED ANALYSIS

(B) SURFACE EROSION: ROADS

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GENERAL ROAD/BASIN INFORMATION

The potential for surface erosion from forest roads varies considerably and is dependent on location or layout, construction practices, drainage, and use. Soil particles on road surfaces, ditches, cutbanks, and fills are entrained by raindrop impact and the shear stress imparted by water flowing in sheets and rills. Erosion from road surfaces is extremely sensitive to traffic levels which produces sediment by the pumping of fines from the substrate through the surfacing and breakdown of surfacing materials. Heavily trafficked logging roads have been shown to produce substantially more sediment than abandoned or low-use roads. Road sediment is mobilized during most rainfall events and snowmelt and can be considered a chronic as opposed to an episodic fine sediment source, such as mass wasting, streambank erosion, or remobilization of channel-stored sediments. Road sediment produced from lightly trafficked roads will decrease during the rainfall season as available fines are winnowed from the tread and ditches. Sediment introduced into stream channels from road surface erosion is assumed to be 2 mm or finer (Duncan et al., 1987; Reid, personal communication, 1989).

Road density in the Tolt is considered to be of significant quantity for field analysis according to the Level 1 screen (greater than 1 mi/mi²). The basin-wide road density is approximately 3 mi/mi² but varies within sub-basins (see road density graph and Road Density/Sediment Summary).

Surface erosion potential from Tolt River watershed roads is in general dependent on two main variables: 1) the percent of road runoff/sediment directly deliverable to streams, and 2) the type and amount of traffic. Deliverability is influenced by the location of the roads in either the westerly lowland area or the easterly highland area. The topography unique to each area dictates similar road construction and drainage patterns. For the purposes of this analysis, the watershed has been divided by lowland and highland areas and by subbasins within these areas.

Roads in the lowland areas are generally lower gradient with fewer stream crossings due to lower topographic relief and a lower stream density in the glacial deposits underlaying most of this area. Lowland roads also parallel a number of wetlands and low gradient stream reaches. Roads here are older than highland roads, and cutbanks and fillslopes are generally well vegetated. Where ditches had not been recently cleaned, most were grass-lined indicating that ditch erosion is not active. The majority of high-use mainline roads are in the lower portion of the basin.

Highland area roads are younger than the lowland roads, are built on steeper slopes, and hence have larger and more frequent cutbanks and fillslopes with less vegetation. The drainage density in the highlands is greater and consequently road drainage delivery to streams will be greater as well. Surfacing varies by availability and is absent on some roads and consists of crushed ballast on others. These are mainly CAT built roads with lots of side cast. A high frequency of fill slope failures has initiated road maintenance measures. Management has been periodically pulling back fill on roads with tension cracks and replacing culverts. Most roads are heavily waterbarred annually, a practice began three years ago. Some sections of road have been put-to-bed with full side-cast pull back.

ANALYSIS METHOD

Road erosion details presented in this report contain a mix of detailed, site-specific information for those road segments field sampled and generalized information on portions of the road system considered particularly problematic. Areas of concern for fine sediments were targeted for field surveys. In addition, all mainline roads north of the South Fork and west of Dry Creek and segments in the light truck, light general use, and non-use categories were field surveyed for estimates of sediment contributions. The distribution of surveyed roads by area and road class are tabulated in the Road Survey Summary.

Snow proved to be a limiting factor to surface erosion analysis at this time of year. Winter blow-down limited road access in the northern portion of the watershed. A helicopter flight of the entire basin provided additional perspective.

Field personnel included Mary Raines, Weyerhaeuser consultant, Nancy Sturhan, DNR soils scientist, and Julie Montalvo, a Weyerhaeuser sub-contractor under the direction of M. Raines. Active observers/advisors to the process included Michael Bonoff and Sandra Donnelly with the Seattle Water Department, Garrett Jackson, consultant for the Seattle Water Department, Sue Perkins and Lori Druffel with King County Surface Water Management, and Kate Sullivan, Weyerhaeuser hydrologist.

Field surveys were similar to Level 1 methods except that every runoff/sediment entry point on a surveyed road segment was evaluated individually for sediment contribution. A different field form was used to aid in recording delivery potential. Road segments field checked are indicated on a paper map of the road system. Roads where detailed surveys were conducted are traced in red pencil and labeled with site numbers corresponding to field notes. Roads traced in blue are those where no sediment contributing road problems were observed or a more cursory, Level 1 survey was conducted.

Field forms and road erosion calculation worksheets are included with this report. Erosion worksheets from the detailed surveys include a calculation of estimated road sediment delivered to streams from each crossing in tons per year, in addition to an average rate of sediment in tons/road prism acre/year for that road segment. The sediment yield numbers

can be used to flag those crossings or areas generating the most sediment, and the rates were used to extrapolate sediment yield estimates to similar roads in the basin not surveyed. The basic erosion rates and corrections made for local conditions from the Level 1 method were used in estimating all sediment yields and rates.

The majority of roads in the upper North Fork and upper South Fork sub-basins were considered similar enough in construction and topography to treat as a group. Limited field surveys were conducted in relatively snow-free segments of the mainline, a low elevation spur, and 65% of the road paralleling the reservoir. The remainder of roads were evaluated for sediment potential by characterizing roads based on interviews with road managers Steve Anderson and Reid Sims from Weyerhaeuser and the Seattle Water Department respectively.

Following the field work and interviews with management, road classes representative of basin roads were selected, and erosion rates were assigned from either averaging rates from similar segments from the field surveys or generating rates based on general road conditions estimated from interviews with managers, the helicopter flight survey, and aerial photographs. The assigned rates were then used to estimate total annual sediment yield from Tolt roads by sub-basin and road class.

For comparison and analysis purposes, the watershed was divided into the following subbasins based on drainage and similarity of roads:

Lower mainstem Tolt Lowland
Stossel Creek Lowland
Lower North Fork Lowland

Yellow Creek Mix of low and highland

Upper North Fork Highland
South Fork below the dam Lowland
South Fork above the dam Highland

The detailed surveys were conducted on sample roads in the same manner as we would assume would be done for the entire road system as part of a comprehensive road management plan. Road surveys will assess sediment delivery and identify problem locations on all road segments for the purpose of prioritizing maintenance and rehabilitation work.

ANALYSIS RESULTS

All road segments, with the exception of the south reservoir road, ranked Low in overall road erosion hazard according to the manual method ranking; however, individual crossings fell in high, medium, and low rankings when calculated separately. Road surface erosion Map bb-2 reflects the overall ratings. The low overall hazard ratings for individual road segments are driven mainly by the low deliverability of roads in the lowland areas and lower

traffic levels in the highland areas.

Map bb-2 also shows the location of known road hazard areas determined from the field surveys and problematic road systems or areas determined from interviews with management, the flight survey, and aerial photographs. The attached list provides a description of the fine sediment/surface erosion condition at each site or area by road erosion number (RE #). Detailed road surveys will need to be completed to identify site-specific problems on non-surveyed roads.

Estimated road sediment yield for each sub-basin by road class is summarized in the following sub-basin sediment summary tables and in the Road Density/Sediment Summary. The most significant results are summarized as follows:

- 1. The total estimated annual fine sediment delivered to streams in the Tolt Watershed is 9,360 tons.
- 2. Although the total length of basin roads is equally divided between the lowland and highland, 75% of the annual sediment yield is generated from highland roads despite the lack of mainline road in this area.
- 3. Road maintenance measures aimed at reducing sediment delivery to streams could have a significant impact on total sediment yield. For example, the highland road sediment estimate could be reduced by 1750 tons annually by decreasing the overall delivery rate from the estimated 33 percent to 25 percent, which means diverting 8 percent of the road drainage to non-contributing areas.
- 4. Roughly 50% of the basin sediment yield is generated from highland general-use roads alone, which includes the problematic Titicaca and Bobcat Creek systems in addition to 70 miles of general use road with an estimated 33% delivery rate. 31% of basin roads fall in the highland general use category.
- 5. The South Fork sub-basin above the dam has the highest sediment per mile rate of 62 tons. A high delivery rate from the disturbed south reservoir road contributes significantly to this number.
- 6. In the lowland, mainline roads contribute 21% of basin sediment from 9% of basin roads.
- 7. Yellow Creek has the third highest road sediment rate due to the mix of both highland and lowland topography.
- 8. Stossel Creek has the highest lowland road sediment rate due to a high road density and length of deliverable mainline road.

- 9. Lower Mainstem Tolt road sediment rate is the lowest in the basin at 2 t/road mile due to low road density, low deliverability of road sediments, and low traffic use.
- 10. Theoretically, the total annual basin sediment yield from roads could be reduced by 16% (1500 tons) by closing off all general use roads to traffic.

Additional analysis interpretation is provided for specific areas under the general comments below.

CONFIDENCE IN ANALYSIS

Experience from road surveys indicates that individual road crossings may locally generate a disproportionate amount of sediment, and it is expected that for most roads this would be the case. These conditions have been averaged into the survey samples and are reflected in the estimated rates used for the unsurveyed roads. Estimates of erosion rates for two highland road segments revised following subsequent physical surveys were adjusted by a factor of 4, affecting total highland sediment estimates by 37 percent. Sediment rates and adjusted estimates are within the order-of-magnitude accuracy assigned to this type of analysis and justify moderate to high confidence levels in predicting relative rates of sediment generated from road surface erosion.

Site-specific erosion problems are limited to those road segments that were field surveyed. The larger the field sample of roads and road classes within the total, the higher the confidence will be in identifying specific factors contributing to surface erosion common to entire road systems, either due to physical characteristics or road construction practices. An example of this is, as a result of limited highland surveys, we determined that highland ditches carry a lot of runoff from cutbanks and slopes where ditches in the lowland areas function mainly to drain the roads.

Confidence in identifying general road characteristics and the relative amount of sediment contributions from different road classes in the lowland portion of the basin is high. 81 percent of mainline, high-sediment-contributing roads were field checked (see Road Survey Summary). Secondary or light truck traffic use roads were also well represented in the sample. Light general and non-use lowland roads surveyed constitute 6 and 3 percent of those totals. Although the lower traffic use roads are under-represented in the sample, the general topography and road construction practices common to all lowland roads were well-sampled within the higher-use categories.

Confidence in evaluating surface erosion from highland roads is moderate for identifying general road characteristics for estimating sediment rates, and low for identifying specific causal mechanisms of erosion. General road characteristics have been adequately described, but the most significant unknown is the percentage of sediment delivery. Changes in estimated road widths, cutbanks and fill vegetation, and ditch armoring would potentially

make less difference in the estimates. In the absence of field data, road sediment delivery in the upper North and South Forks was estimated at 33% for most roads, an empirically derived average from studies in similar harvested environments (Sullivan et al., 1989, Raines, 1991) and 10% for roads put-to-bed. Road maintenance measures may have reduced the 33% empirical average. Confidence in the sediment estimates would improve from moderate to high upon field sampling for delivery and general road characteristics.

Confidence in identifying causal mechanisms of highland road surface erosion will increase from low to moderate and high with adequate field sampling. With the current level of field checking and management information, suspected causal mechanisms of erosion include direct delivery rates to streams, variable surfacing, intercepted slope drainage, slope instability, unvegetated cuts and fills, traffic levels, and high road gradients. Erosion may also occur because of the lack of adequate water drainage due to ditch infilling or inadequate inboard ditches and relief culverts. Water building up on the road surface will overload the existing drainage facilities resulting in gullying and fill failures.

Sediment estimates indicate that 50% of Tolt basin road sediment is potentially generated from the 94 miles of highland general use roads, which suggests a diffused source. Only 2.3% of these roads have been surveyed. Field surveys on these roads will help focus maintenance efforts.

NEW ROAD CONSTRUCTION

Planned road construction totals approximately 7.2 miles within the next 3 years (93-95). Weyerhaeuser management has not planned new roads beyond 1995 at this time. All of these roads are short spurs off of existing road systems and lie entirely within the lowland area. The locations of planned roads are marked in red on the road surfacing and use information map provided by Weyerhaeuser. The time distribution of construction within the 3 year period is not known, but assuming all 7.2 miles are built the same year with an average 30 foot road prism width and 15% delivery rate and heavy log truck traffic during the first year, increases in sediment yield are estimated as follows:

| | Traffic Use | ER Rate | ER 15% Delivery | Est. Annual Sed. Yield |
|---------|----------------|------------|--------------------|------------------------|
| Year 1 | H | 110 | 16.5 | 430 tons |
| Year 2 | G | 41 | 6.1 | 160 tons |
| Year 3+ | G | 29 | 4.4 | 115 tons |

The increase in basin road sediment yield is estimated at approximately 4-5% during the first year of construction, decreasing to 1% by year 3. The delivery rate has been estimated conservatively based on delivery rates off the mainline in the lowland area. Many of the planned spur roads will be non-contributing due to flat, terrace locations and non-proximity

to streams. Vegetation of cutbanks and fill slopes will contribute to a decreasing rate after year 3.

Distribution of the planned 7.2 miles of new road by lowland sub-basin is listed on the sub-basin sediment summary sheets.

LOWLAND ROADS

The Lower Mainstem Tolt sub-basin has the lowest road density in the watershed, and the lowest estimated sediment contribution from logging roads at 52 t/yr total. In addition, road usage which drives sediment rates up is limited to light general traffic on the logging roads and an asphalt county road. No mainline or secondary roads are located in the lower mainstem. Observed roads were lightly trafficked and had relatively low gradients. Localized problems may occur in areas frequented by local traffic near the town of Carnation.

The majority of sediment from roads in Stossel Creek is generated from the mainlines due to the heavy truck traffic (479 t/yr mainline out of 578 t/yr total). Relief culverts drain much of the mainline road that parallels the stream, but only 2 out of 16 were determined to deliver water and sediment to the stream. More sediment is generated from the pipeline mainline road through Stossel Creek than the Stossel Creek mainline. The road tread is generally wider on the pipeline, and long grades drain directly to crossings with little relief in between. Surfacing on the pipeline road suffers more from the high traffic levels than other parts of the mainline. The tread becomes deeply rutted during rainfall, and a plume of sediment from road ditch runoff was photographed entering the stream downstream of the crossing at field site #4. The cause of the rutting is likely due to the till parent material here, which is high in fines. Opportunities for entry exist at all stream crossings and where the road is within 100 feet of the stream. Roads occasionally parallel wetlands or streams in other parts of the lowland basin area, but the Stossel Creek road system is unique in the amount of road paralleling streams.

Except for the pipeline road through Stossel Creek, mainline surfacing appears adequate, although fines are abundant and easily airborne. The volume of fines available is to be expected from the heavy truck traffic, but it is unclear if the fines are generated from breakdown of the surfacing material or from fines pumping through the surfacing from the glacial parent material in the non-till areas.

Detailed road surveys were not conducted in the North Fork Creek drainage. Road density in this drainage is noticeably lower than in other portions of the lowlands, and the main secondary road is generally well buffered from streams. Experience from other road surveys would indicate that individual road crossings may locally generate a disproportionate amount of sediment, and it is expected that this road system would be similar. Road sediment

delivery is highest from the mainlines in the lowlands, which are limited to singular stream crossings outside the Stossel Creek, North Fork and Crazy Creek areas.

Most of the surface drainage from the lower South Fork sub-basin flows from the Lynch Creek system. The large majority of sediments delivered to streams in the South Fork are from mainline road crossings, which account for virtually 87% of the total (727/833 t/yr). The majority of mainline entry points occur on Crazy Creek.

A significant obstruction to flow in Lynch Creek is located upstream of Lynch Lake at a failed road crossing.

HIGHLAND ROADS

The only roads above the dam field surveyed were portions of the north and south reservoir roads. A rough sediment budget of road surface sediment delivered from roads suggests that as much as 2400 t/yr is generated from roads. Background fine sediment input to the reservoir is estimated roughly at 1000 t/yr, indicating that roads may contribute two times as much sediment.

A contrast exists between the two reservoir roads. The T70 road appears to be the older or more stable road, with evidence of railroad logging and a number of log culverts and stream crossings, many of which were only partly functioning. Sediment is delivered to the reservoir from approximately 40 percent of the road. Both reservoir roads are located at the toe of the slope with evidence of groundwater and both channelized and unchannelized overland flow from the hillslopes and cutbanks above the roads draining to road culverts, ditches, and road surfaces.

Vintage large, non-corregated iron pipe have been used for culverts on the 50 reservoir road. The only wooden structure in place observed was a log bridge spanning Skookum Creek. Replacement of log culverts and crossings may have been necessary due to the high maintenance obvious on the road. Evidence of 5 debris events from streams has impacted the road recently, and necessaray maintenance activities keep the surfacing disturbed. The 50 road surface is mainly outsloped yet a grading berm allows concentration on the tread, and the close proximity of the road to the water essentially guarantees close to 100 percent delivery of runoff and sediment. The road was impassable 2.8 miles from the dam due to a debris event. This section of road is currently seeing increased traffic levels due to crossing failurers on the eastern portion of the road system surrounding the reservoir, and the segment was evaluated at a light logging truck rate. A lighter traffic level would reduce the estimate by 50 to 75 percent.

The Bobcat Creek road system was estimated to contribute a higher percentage (32%) of sediment than other parts of the sub-basin, in part due to the natural instability of the terrain, steeper slopes and road gradients. Sediment delivered to streams from these roads

is estimated to be equivalent to a loss of 0.3 inches/yr from the road tread, ditches and cutbanks.

South aspect roads are generally in better shape than north aspect roads on both upper North and South Forks due to gentler slopes, relatively fewer stream crossings, and a greater length of road put-to-bed with full side-cast pulled back.

The Titicaca system corresponds topographically and aspect-wise with the Bobcat Creeks roads in the upper South Fork. Both systems experience road maintenance problems. A number of fill slope failures have initiated debris flows from these roads. Roads here have been water-barred for the last three years, and management tries to get to them twice a year. Delivery was not field checked and is assumed to be 33%. A thorough field inventory will help determine the effectiveness of waterbars in diverting road sediment from streams. Waterbars currently relieve the ditches.

The road system in the Titicaca basin was treated differently from the remaining upper North Fork roads with respect to estimating road sediment delivery. These are the youngest roads in the sub-basin being in the least accessable and steepest ground in the watershed, so cutbanks and slopes have less vegetation and the road gradients are steeper. An estimate of road sediment delivery indicates approximately 37% of upper Nork Fork road sediment is potentially generated from these roads.

Because there are close to 50 miles of light general use roads in the upper North Fork area, these roads collectively contribute the same amount of sediment annually as the Titicaca road system: approximately 37% of the estimate or 1670 tons. Additionally, 25 miles of non-use roads contribute roughly 580 tons or 13%. Mainlines contribute approximately 350 tons. The total of annual road sediment from the upper North Fork is estimated at 4500 tons.

CHANGING TRAFFIC LEVELS

Heavy traffic is expected to continue on the mainline roads. The existing road system, however, will experience a shifting use pattern dependent on harvest, maintenance, and recreational activities.

Changes in road sediment rates from alternative traffic use scenerios are tabulated on the road erosion worksheets (Form bb-3) for each road segment surveyed. The majority of roads were surveyed by calculating sediment yield for each entry point on the road. Worksheets for these surveys show changes in sediment rates under heavy traffic (>4 loaded logging trucks/day) and light traffic (1-4 loaded logging trucks/day) use conditions for each entry point rather than the change in rate averaged over the entire road segment on the remaining surveys.

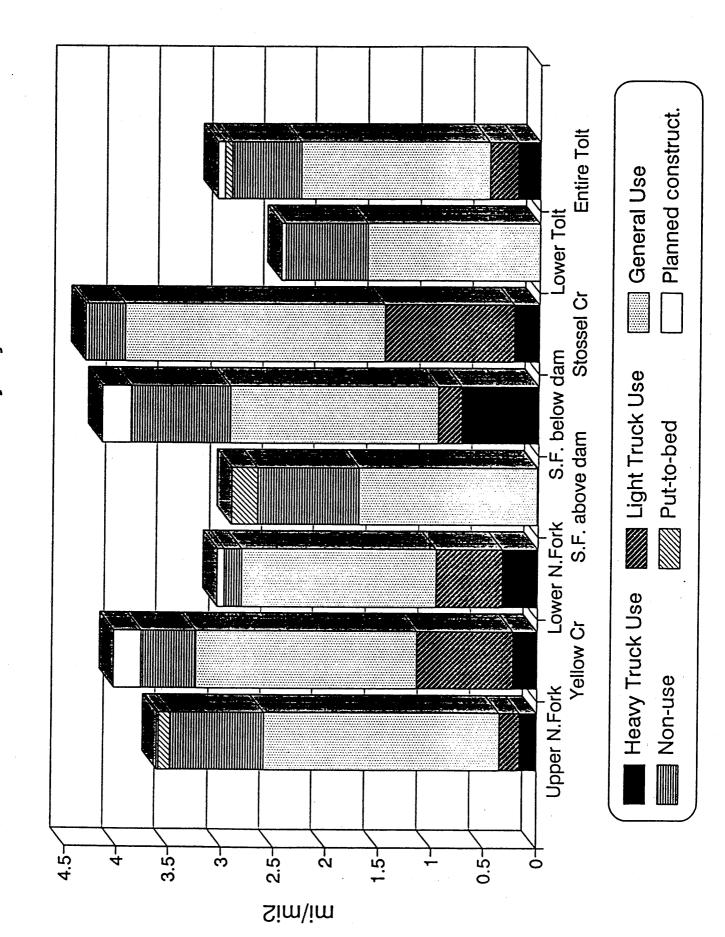
Increasing traffic levels from light truck use to heavy truck use increases sediment erosion rates by a factor of 7 to 10. Increasing general use traffic will affect an erosion rate increase by a factor of approximately 15 for heavy use and 2 to 4 for light truck use.

Road managers can use the estimated and projected rates to predict the change in road sediment with changing traffic use patterns.

As stated in above, theoretically, the total annual basin sediment yield from roads could be reduced by 16 percent (1500 tons) by simply closing off all general use roads to traffic. Although closing all roads may not be practical for fire and other access, this example illustrates the importance of traffic use in road surface sediment production.

REFERENCES

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- Raines, M. A., 1991, Sediment budget for the Grouse Creek basin, Humboldt County, California, M.S. Thesis, 110 pp., West. Wash. Univ., Bellingham.
- Sullivan, K., et al., 1989, The generation and fate of road surface sediment in forested watersheds in Southwestern Washington, <u>Forest Science</u>, 35(2), pp. 453-468.



TOLT WATERSHED ANALYSIS Road Survey Summary

| | | Miles | Percent | Percent of | Estimated | Percent of |
|------------------|----------|---------|----------|------------|-----------|---------------|
| | Miles | in Road | Roads | Tolt Roads | Sediment | Est. Sediment |
| Road Class | Surveyed | Class | Surveyed | in Class | (t/yr) | Total |
| | | | | | | |
| Lowland | | | | | | |
| Mainline | 21.3 | 26.2 | 81 | 9.8 | 1959 | 20.9 |
| Secondary | 11.1 | 14.5 | 9/ | 4.8 | 180 | 1.9 |
| Light general | 5.5 | 85.9 | 6.4 | 28.2 | 197 | 2.1 |
| Non-use | 0.76 | 25 | 3 | 8.2 | 30 | 0.3 |
| | | | | | | |
| Lowland Totals | 38.7 | 151.6 | 25.5 | 49.7 | 2366 | 25.3 |
| | | | | | | |
| Highland | | | | | | |
| Mainline | 0 | 0 | 0 | 0.0 | 0 | 0.0 |
| Secondary | 2.8 | 12 | 23 | 3.9 | 1294 | 13.8 |
| Light general | 2.2 | 93.8 | 2.3 | 30.8 | 4502 | 1.67 |
| Non-use | 0 | 41.1 | 0 | 13.5 | 1050 | 11.2 |
| Put-to-bed | 0 | 6.7 | 0 | 2.2 | 58 | |
| | | | | | | |
| Highland Totals | 5 | 153.6 | 3.3 | 50.4 | 6994 | 74.7 |
| Watershed Totals | 43.7 | 305.2 | 14.3 | 100 | 9360 | 100 |

| | | Basin | Road | Est. | Sediment | Sediment |
|---------------------|-------|-------|----------|----------|----------|-----------|
| | Road | Area | Density | Sediment | Per Area | Per Mile |
| Sub-basin | Miles | (mi2) | (mi/mi2) | (tons) | (t/mi2) | (t/rd mi) |
| | | | | | | |
| S. Fork above dam | 38.8 | 19 | 2.0 | 2404 | 127 | 62 |
| Upper N. Fork | 105.5 | 33.1 | 3.2 | 4495 | 136 | 43 |
| Yellow Cr | 18.7 | 4.9 | 3.8 | 553 | 113 | 30 |
| S. Fork below dam | 50.2 | 12.9 | 3.9 | 833 | 65 | 17 |
| Lower N. Fork | 37.5 | 12.4 | 3.0 | 448 | 36 | 12 |
| Stossel Cr | 23.1 | 5.1 | 4.5 | 578 | 113 | 25 |
| Lower Mainstem Tolt | 31.3 | 10.5 | 3.0 | 52 | 5 | 2 |
| Watershed Totals | 305 | 98 | 3.1 | 9363 | 96 | 31 |

TOLT WATERSHED CAUSAL MECHANISM REPORT 4/1/93

Known Road Hazard Areas:

- RE 1 Highest contributing road crossing on Stossel Cr mainline. Road here bisects and parallels stream and wetland area. No relief culverts and almost 1000 feet of 8-10% grade draining either directly or indirectly to stream. Heavy traffic. Segment site #2 on field form.
- RE 2 Relief culvert draining a 500' length of 10% road grade is perched directly above Index Creek immediately upstream of the 6170 road crossing. Light truck traffic road. Segment site #5 on field form.
- RE 3 Section of 6170 road below the Index Creek crossing parallels the stream and wetland within a few feet. The road has been ditched closed due to garbage dumping occurring here in and near the wetland. Sediment due to traffic minimized with road closure, but garbage still in water.
- RE 4 Two road segments drain to Index Creek tributary from over small fill at this crossing. Segment site #11 on field form.
- RE 5 Recently reconstructed segment of road immediately adjacent to Stossel Creek wetland. Road requires lots of ballast to keep from sinking. Limited direct entry due to concave nature, but road lacks drainage for most of length. No cutbanks or fill slopes. This segment is an extension of the mainline and may see heavy truck traffic.
- RE 6 Long length (1200') of high gradient mainline/pipeline road drains to tributary that joins Stossel Creek near the mouth. Fines from road surface likely to stay in suspension although there is good vegetation on road margins and fillslopes to trap coarser particles. Segment site #2 on field form.
- RE 7 Small creek diverted into ditch; culvert insufficient. Segment site #5 on pipeline-mainline field form.
- RE 8 Ditch draining segment west of crossing below the road is gullied to the stream. Mainline/pipeline road. Segment site #6 on field form.
- RE 9 400' segment of mainline road draining to stream from ditch. Road is crowned or outsloped but entire outsloped edge is bermed allowing water to concentrate at crossing. Segment site #3 on field form.

- RE 10 Lynch Creek: one of the two culverts plugged under washed-out crossing. Stream flows down road intermittently for approximately 1000 feet. Road is in non-use and most sediment has already been eroded from the road surface, but the water would more likely stay in the channel if the culvert was unplugged or removed. Road has insufficient lift. New road construction is expected at or near this crossing within the next few years. Site #1 on field form.
- RE 11 Lynch Creek culvert at crossing aimed at and eroding opposite bank of stream. Crossing drains 3 road segments. Site #2 on field form.
- RE 12 Long length (2100') of mainline road, crowned surface with ditch draining to Crazy Creek. Road has grading berm funneling some surface runoff through breach on upstream side. Sediment is ponded below the breach on a flood terrace above the active stream channel, which is probably inundated at high flows. Site #3 on field form.
- RE 13 Gullying along length of access road to lower dam from water draining from T70 mainline. Direct entry checked on 3/22. Road drainage runs for several thousand feet on terrace surface, sometimes channelized sometimes not, but eventually infiltrates dropping sediment along the way. Contributes to some degree to groundwater seeps off sand cliff face above the South Fork on the right bank terrace below the dam. Runoff from approximately 0.5 mile of road and large helicopter landing site drains to this point. Site #1 on T70 road field form.
- RE 14 Road paralleling reservoir within 200 feet constructed on alpine glacial outwash. 50 road field survey shows a 40 percent delivery rate. Old log culverts and crossings non or partially functional in places. Ditches filled with sediment from upslope in some places.
- RE 15 Road paralleling reservoir within 200 feet constructed on andesite. Native surfacing in places. Delivery estimated at 95 percent from field checking. This section of road is currently seeing increased traffic levels due to crossing failures on the eastern portion of the road system surrounding the reservoir. Evidence of 5 debris events from streams is impacting the road, and necessary maintenance activities keep the surfacing disturbed. Road impassable 2.8 miles from dam due to culvert failure and debris event.
- RE 16 Bobcat Creek road system. Eastern-most roads in the upper South Fork built in the late 70's on steep, north aspect slopes. Natural slope instability, steep road gradients, steep and unvegetated cutbanks and fills, and necessary road drainage maintenance activities contribute to chronic sediment production.
- RE 17 Long length (1000') of mainline road drains to stream. Site #1 on field form.
- RE 18 Long length (800') of mainline road drains to stream from road surface and ditch. Site #5 on field form.

- RE 19 This section of mainline road is problematic. Active bank erosion on the north side of the river is creating bank instability where the road parallels the stream here. There may be a component of road drainage contribution to the problem. Field form site #6 has high direct entry potential and possibly contributes to downstream bank erosion in small stream from increased runoff. Sites #6,7, and 8 on field form.
- RE 20 90 road crossing fill is failing. Some fill loss already occurred and entire fill subsiding. Cause indeterminant due to snow. Site #2 on field form.
- RE 21 92 road segment. Water flowing over road between field sites #3 and 4. Road crossing completely washed out at site #4. Failure of old log crossing.
- RE 22 Mid to lower-slope roads on steep slopes. Road less than 10 years old. Side cast is not well vegetated. Several slope failures initiated from roads.
- RE 23 Stacked road system above Winter Lake. Cutbank and fill failures, and banks and fills not well vegetated. Delivery to streams or water is uncertain, needs field checking.
- RE 24 Road 130 crossing. Road built on alluvial fan. The crossing has been replaced several times, the last with a structural steel bridge.
- RE 25 Titicaca road system, similar to Bobcat Creek roads. Roads built in the 80's on steep, north aspect slopes. Natural slope instability, steep road gradients, steep and unvegetated cutbanks and fills, and necessary road drainage maintenance activities contribute to chronic sediment production.
- RE 26 Titicaed Creek roads. Cut banks from long grade on west side of creek intercept much groundwater adding to the road surface runoff in addition to cutbank and ditch erosion. Maintenance has re-sized culverts to 3' to handle flow. Raveling of fill slopes on east side of stream.

Sub-basin:

South Fork above dam

3/24/93

| | Erosion | Erosion | | Road | Road | Est. Sediment |
|--------------------------|---------|---------|-------|-------|-------|---------------|
| | Rate | Hazard | Road | Prism | Prism | Yield |
| Road Class | t/ac/yr | H/M/L | Miles | Width | Acres | t/yr |
| Lowland roads | | | | | | |
| Mainlines | 20.6 | J | | 30 | 0.0 | 0 |
| Secondary | 2.4 | 7 | | 30 | 0.0 | 0 |
| Light general | 0.5 | ı | | 25 | 0.0 | 0 |
| Light general-new | 1.5 | J | | 25 | 0.0 | 0 |
| Non-use . | 0.4 | 7 | | 25 | 0.0 | 0 |
| To be built | | | | | | |
| Highland roads | | | | | 0.0 | 0 |
| Secondary | 9.6 | ı | 0.1 | 30 | 0.4 | 9 |
| Light general | ∞ | 1 | 9.6 | 35 | 40.7 | 326 |
| Reservoir s rd-andesite | 77 | × | 3 | 35 | 12.7 | 086 |
| Reservoir rd-alluvium | 4 | u | 3.5 | 35 | 14.8 | 59 |
| Non-use | 5.4 | ı | 10.4 | 35 | 44.1 | 238 |
| Put-to-bed | 2 | J | 3.2 | 35 | 13.6 | 27 |
| Titicaca & Bobcat Cr rds | | | | | - | |
| Light general | 20 | J | 6.2 | 40 | 30.1 | 601 |
| Non-use | 13.7 | J | 2.5 | 40 | 12.1 | 166 |
| Put-to-bed | 2 | J | 0.3 | 40 | 1.5 | e |
| | | | | | | |

2404

170

38.8

Sub-basin:

Upper North Fork

| | Erosion Rate | Erosion Hazard | Road | Road Prism | Road Prism | Est. Sed. Yield |
|--------------------------|-----------------|-------------------|-------|---------------|---------------|--------------------|
| Road Class | t/ac/yr | H/M/L | Miles | Width | Acres | t/yr |
| Lowland roads | | | | | | |
| Mainlines | 20.6 | H | 4.7 | 30 | 17.1 | 352 |
| Secondary | 2.4 | ı | | 30 | 0.0 | 0 |
| Light general | 0.5 | 1 | | 25 | 0.0 | 0 |
| Light general-new | 1.5 | J | | 25 | 0.0 | 0 |
| Non-use | 0.4 | □ | | 25 | 0.0 | 0 |
| To be built | • | | 0.7 | | | |
| | | | | | | |
| Highland roads | | • | | | | |
| Secondary | 9.6 | H | 5.9 | 30 | 21.5 | 206 |
| Light general | 8 | J | 49.1 | 35 | 208.3 | 1666 |
| Reservoir rd-andesite | 19 | H | | 35 | 0.0 | 0 |
| Reservoir rd-alluvium | 15 | ъ. | | 35 | 0.0 | 0 |
| Non-use | 5.4 | J | 25.5 | 35 | 108.2 | 584 |
| Put-to-bed | 2 | H | 2.6 | 35 | 11.0 | 22 |
| Titicaca & Bobcat Cr rds | | | | | | |
| Light general | 20 | ᆸ | 17.1 | 40 | 82.9 | 1658 |
| Non-use | 13.7 | u | | 40 | 0.0 | 0 |
| Put-to-bed | 2 | J | 9.0 | 40 | 2.9 | 9 |
| | | | | | | |

4495

452

106.2

Sub-basin:

Yellow Creek

| IIOISO III | Erosion | , | Road | Road | Est. Sed. |
|------------|---|-------|--|---|--|
| Rate | Hazard | Road | Prism | Prism | Yield |
| t/ac/yr | H/M/L | Miles | Width | Acres | t/yr |
| | | | | | |
| 20.6 | J | 1.1 | 30 | 4.0 | 82 |
| 2.4 | u | 1.5 | 30 | 5.5 | 13 |
| 0.5 | ٦ | | 25 | 0.0 | 0 |
| 1.5 | H | 2.1 | 25 | 6.4 | 10 |
| 0.4 | ٦ | | .25 | 0.0 | 0 |
| | | 1.3 | ٠ | | |
| | | | | | |
| 9.6 | J | 3.0 | 30 | 10.9 | 105 |
| 8 | u | 8.3 | 35 | 35.2 | 282 |
| 19 | H | | 35 | 0.0 | 0 |
| 15 | ٦ | | 35 | 0.0 | 0 |
| 5.4 | 니 | 2.7 | 35 | 11.5 | 62 |
| 2 | H | | 35 | 0.0 | 0 |
| | | | | | |
| 20 | 니 | | 40 | 0.0 | 0 |
| 13.7 | u | | 40 | 0.0 | 0 |
| 2 | H | | 40 | 0.0 | 0 |
| П | Rate t/ac/yr 20.6 2.4 0.5 1.5 0.4 9.6 8 19 15 15 17 18 13.7 | | Hazard Roi H/M/L Mii L L L L L L L L L L L L L | Hazard Road H/M/L Miles L 1.1 L 1.5 L 2.1 L 3.0 L 8.3 L 2.7 L L 2.7 L L L 1.3 | Hazard Road Prism H/M/L Miles Width L 1.1 30 L 2.1 25 L 2.1 25 L 3.0 30 L 8.3 35 L 8.3 35 L 2.7 35 L 2.7 35 L 40 L 40 L 40 |

553

73

20.0

TOLT WATERSHED ANALYSIS Road Sediment Summary

Sub-basin:

Stossel Creek

| | Erosion | Erosion | Dond | Road | Road | Est. Sed. |
|--------------------------|---------|-------------|-------|-------|-------|----------------|
| Road Class | t/ac/yr | H/M/L | Miles | Width | Acres | r leid t/yr |
| Lowland roads | | | | | | |
| Mainlines | 20.6 | 7 | 6.4 | 30 | 23.3 | 479 |
| Secondary | 2.4 | ٦ | 1.1 | 30 | 4.0 | 10 |
| Secondary-rebuilt | 35.9 | J | 0.95 | 15 | 1.7 | 62 |
| Light general | 0.5 | J | 10.8 | 25 | 32.7 | 16 |
| Light general-new | 1.5 | ٦ | 1.9 | 25 | 5.8 | 6 |
| Non-use | 0.4 | ٦ | 1.9 | 25 | 5.8 | |
| To be built | | | 0.5 | · | | |
| | | | | | | |
| Highland roads | | | • | | | • |
| Secondary | 9.6 | u | | 30 | 0.0 | 0 |
| Light general | ∞ | 니 | | 35 | 0.0 | 0 |
| Reservoir rd-andesite | 19 | רו י | | 35 | 0.0 | |
| Reservoir rd-alluvium | 15 | u | | 35 | 0.0 | 0 |
| Non-use | 5.4 | J | | 35 | 0.0 | 0 |
| Put-to-bed | 7 | u | | 35 | 0.0 | 0 |
| Titicaca & Bobcat Cr rds | • | | | | | |
| Light general | 20 | ٦ | | 40 | 0.0 | 0 |
| Non-use | 13.7 | u | | 40 | 0.0 | 0 |
| Put-to-bed | 7 | ı | | 40 | 0.0 | 0 |
| | | | | | | |

578

73

23.3

Sub-basin:

Lower Mainstem Tolt

| | Erosion | Erosion | | Road | Road | Est. Sed. |
|--------------------------|---------|--|-------|-------|-------|-----------|
| | Rate | Hazard | Road | Prism | Prism | Yield |
| Road Class | t/ac/yr | H/M/L | Miles | Width | Acres | t/yr |
| Lowland roads | | | | | | |
| Mainlines | 20.6 | 7 | | 30 | 0.0 | 0 |
| Secondary | 2.4 | 7 | | 30 | 0.0 | 0 |
| Light general | 0.5 | 7 | 20.7 | 25 | 62.7 | 31 |
| Light general-new | 1.5 | ı | 2.2 | 25 | 6.7 | 10 |
| Non-use . | 0.4 | 7 | 8.4 | 25 | 25.5 | 10 |
| To be built | | | 0.5 | | | |
| Highland roads | | 6 to 20 to 2 | | | | • |
| Secondary | 9.6 | 1 | | 30 | 0.0 | 0 |
| Light general | ∞ | u | | 35 | 0.0 | 0 |
| Reservoir rd-andesite | 19 | J | | 35 | 0.0 | 0 |
| Reservoir rd-alluvium | 15 | ı | | 35 | 0.0 | 0 |
| Non-use | 5.4 | 1 | | 35 | 0.0 | 0 |
| Put-to-bed | 2 | H | | 35 | 0.0 | 0 |
| Titicaca & Bobcat Cr rds | | | | | | • |
| Light general | 20 | ı | | 40 | 0.0 | 0 |
| Non-use | 13.7 | u | | 40 | 0.0 | 0 |
| Put-to-bed | 2 | ח | | 40 | 0.0 | 0 |
| | | | | | | |

52

95

31.8

TOLT WATERSHED ANALYSIS Road Sediment Summary

Sub-basin:

South Fork below dam

| | ווחופום ו | Erosion | | Road | Road | Est. Sed. |
|--------------------------|-------------|---------|-------|-------|-------|-----------|
| | Rate | Hazard | Road | Prism | Prism | Yield |
| Road Class | t/ac/yr | H/M/L | Miles | Width | Acres | t/yr |
| owland roads | | | | | | |
| Mainlines | 20.6 | H | 9.7 | 30 | 35.3 | 727 |
| Secondary | 2.4 | u | 3 | 30 | 10.9 | 26 |
| Light general | 0.5 | J | 16.1 | 25 | 48.8 | 24 |
| Light general-new | 1.5 | ı. | 8.9 | 25 | 27.0 | 40 |
| Non-use | 0.4 | ٦ | 12.5 | 25 | 37.9 | 15 |
| To be built | | | 3.6 | | | |
| Highland roads | | | | | | |
| Secondary | 9.6 | 7 | | 30 | 0.0 | 0 |
| Light general | 8 | u | | 35 | 0.0 | 0 |
| Reservoir rd-andesite | 19 | -1 | | 35 | 0.0 | 0 |
| Reservoir rd-alluvium | 15 | ٦ | | 35 | 0.0 | 0 |
| Non-use | 5.4 | 7 | | 35 | 0.0 | C |
| Put-to-bed | 2 | ı | | 35 | 0.0 | · C |
| Titicaca & Bobcat Cr rds | | | - | | • | • |
| Light general | 20 | 1 | | 40 | 0.0 | 0 |
| Non-use | 13.7 | -1 | | 40 | 0.0 | 0 |
| Put-to-bed | 2 | T | | 40 | 0.0 | 0 |

833

160

53.8

TOLT WATERSHED ANALYSIS Road Sediment Summary

Sub-basin:

Lower N. Fork

| Road Class t/ac/yr Lowland roads Mainlines 20.6 Secondary 2.4 Light general Light general-new 1.5 Non-use 0.4 To be built | 6 L 4 | | | 4 4 4 4 4 4 4 | |
|---|-------|-------|-------|---------------|------|
| al al-new | | Miles | Width | Acres | t/yr |
| al al-new | | | | | |
| | | 4.3 | 30 | 15.5 | 319 |
| | | . 8.0 | 30 | 28.9 | 69 |
| | | 15.8 | 25 | 47.7 | 24 |
| | | 7.4 | 25 | 22.3 | 33 |
| To be built | | 2.2 | 25 | 6.7 | 3 |
| | | 0.9 | | | |
| Highland roads | | | | 0 | • |
| | | | | 0 | 0 |
| | | | | 0 | 0 |
| 1-andesite | | | | | |
| Reservoir rd-allluvium 15 | | | | 0 | 0 |
| | | | | 0 | 0 |
| • | | | | 0 | 0 |
| Titicaca & Bobcat Cr rds | u | | | 0 | 0 |
| Light general 20 | | | | 0 | 0 |
| Non-use 13.7 | 7 | | | | |
| Put-to-bed | 2 L | | | 0 | 0 |

448

121.1

38.5

TOLT WATERSHED ANALYSIS CONDENSED ROAD COMMENTS 3/30/93

1. Projected road construction plans and estimated impacts.

Added section on New Road Construction in summary. Includes location and amount of projected road construction with conservative estimates of additional sediment contribution for next 3 years.

2. Incorporation of hillslope surface erosion and mass wasting information into the road analysis.

Comparing the different sources of fine sediment is most appropriate to the synthesis phase. The resource assessment reports would be the likely format for this comparison.

3. Confidence in analysis due to lack of field verification in highland, or estimated increase in confidence with more field time.

Expanded confidence discussion. Split level of confidence in highland to moderate for sediment estimate and low for identifying specific causal mechanisms of erosion.

4. Roads rated low and no consideration given to road density. Level 1 method inadequate for Level 2 and underrepresents potential damage to public resources.

The March 10 summary and supporting tabulations address this directly by focusing the analysis on the cumulative sediment estimated from all roads.

5. Procedure for pending road inventory. (Causal Mechanism Report says "see module report for inventory plan). Incomplete and inadequate road survey; many problem areas missed. How to incorporate future survey to insure results addressed in prescriptions. (In her comments, Sue Perkins suggests that a procedure for handling these areas needs to be discussed with the whole group).

The intention of this analysis is to sample the road system in order to provide causal mechanisms of road erosion specific to the Tolt. Due to weather, the higher elevation areas were not adequately sampled. Wording was added to clarify what information a management road survey would provide and how that information would be used to prioritize maintenance efforts. The review group will wait to see how the prescription team will tie a road survey into the prescriptions.

6. Dominant factors affecting road related surface erosion in the basin.

Wording has been added to emphasize main variables and site-specific factors where we have that information.

7. What is the quantity of road sediment directly delivered to the channel on an annual basis?

Estimates are summarized in the Results section of the write-up and on the Road Sediment Summary sheets for each sub-basin by road class.

8. Distribution of sediment type produced from roads.

Added sentence in first paragraph on sediment sizes measured from road surface erosion.

TOLT WATERSHED Pipeline mainline from 26N7ES26 to Reg. pond m bb-3. Road Erosion Worksheet

Stossel Cr, Lower N. Fork d Segment: -basin:

al Segment Length:

| 9 | ייי טיקיייניי דיייוקייי | = | 20017 | | | | + | | | | + 5.1.2 | | | | EDe + |
|-------|-------------------------|------------|---------|---------|----------|--------|------|---------|------------|-------------|---------|---------|----------|--|-------|
| | | | | | CUISLOPE | 3JC | | | FILLSLOPE | OPE. | | | DIJ | DITCH | |
| Ξ | 3 | ව | (€) | (5) | 9) | Θ | 8 | 8 | (10) | (II) | (12) | (13) | (14) | • | (91) |
| peo | Road | Rock | Basic | Value | 88 | Veg | | Value | 88 | \ \ \ | | Value | Armon | | |
| ment/ | Age | Type | Erosion | ည္ဆ | Vcg | Factor | స్టి | 면 | Veg | Factor | EFe | 60 | χ× | Factor | EDe |
| ije | yrs | | Rate-EB | EB*0.40 | | | | EB*0.20 | | | | EB*0.05 | | | |
| 1 | >3 | Till | 09 | 24.0 | No cut | 0 | 0.0 | 12.0 | 100 | 0.18 | 2.2 | 3.0 🗡 | > | 0.95 | 2.9 |
| 2 | >3 | 111 | 8 | 24.0 | No cut | 0 | 0.0 | 12.0 | <u>8</u> 1 | 0.18 | 2.2 | 3.0 | * | 0.95 | 29 |
| 3 | >3 | 111 | જ | 24.0 | No cut | 0 | 0.0 | 12.0 | 8 | 0.18 | 2.2 | 3.0 | 7 | 0.95 | 2.9 |
| 4 | ×3 | Ice marg. | જ | 24.0 | No cut | 0 | 0.0 | 12.0 | 8 | 0.18 | 2.2 | 3.0 | 7 | 0.95 | 2.9 |
| ~ | 23 | Ice marg. | જ | 24.0 | 75 | 0.37 | 8.9 | 12.0 | IliJou | 0 | 0.0 | 3.0 | 7 | 0.95 | 2.9 |
| 9 | 23 | Till | 9 | 24.0 | 6 | 0.18 | 4.3 | 12.0 | 100 | 0.18 | 2.2 | 3.0 | ٨ | 0.95 | 2.9 |
| - | 2 | Vol/sed rx | ೫ | 12.0 | જ | 0.37 | 4.4 | 0.9 | 001 | 0.18 | 1.1 | 1.5 | 7 | 0.95 | 1.1 |
| 8 | >3 | Vol/sed rx | 30 | 12.0 | 18 | 0.18 | 2.2 | 0.9 | lliJou | 0 | 0.0 | 1.5 | ¥ | 0.95 | 1.1 |
| | | | | | | | | | | | | | | The second secon | 1 |

| 22 2 | 0.2 | 35 35 segment | 17 250 | 17 Total sedii | 109 |
|------------------|-------|---------------------|---------|-------------------|-----|
| 88 | 0.4 | 35 | 200 | 8 | |
| 31 | 0.1 | 39 | 200 | 33 | - 1 |
| 41 | 0.2 | 8 | 350 | 21 | |
| 69 | 0.4 | 35 | 200 | 21 | |
| 145 | 1.0 | 35 | 1200 | 18 | |
| 81 | 0.3 | 35 | 400 | 18 | |
| tons/yr | Acres | Width/ft | ۳ | Traffic | |
| Sediment | Prism | Prism | Length | Ľģř. | |
| Road | Road | Road | Segment | ER | |
| (K) | (33) | (32) | (16) | (30) | l |
| ` | | | | SAMING | ≤ا |

| Cours Preses | DRAIN DITEM | BELLE COS | Je smins at | Cuss / Sioz 0: |
|--------------|-------------|-----------|-------------|----------------|
| #6 | | | | |

HML 172 151 8.0 0 0.7 9.0 0.7 0.7

Overall ER Rate t/ac/yr ERd

Hazard Rating

■ ER

x ERd

(ETe x Use = ETec)

SURFACING

(97)

Direct Entry %/100 Factor 0 | 2

(24) Buffer ERe 8

210.0 ETec Factor

(3)(21) Use (20) Road Ş

ETe (19) (18)

4.2 Surface Factor

(17) Value ET

4.2 4.2 0.2 0.2 EB*0.35 21.0 21.0 21.0 21.0

105.0 ន ន

4.2

0.2

10.5 10.5

210.0 210.0

215 222

215 210.0 210.0 8888

219

222 112

172

8.0 9: 1.0 1:0

8.0

Otal Segment ER =

0:1

Form 1. Road Segments Para...hmg Streams Within 200 Ft.

codes 150' I'mt -. Center 360 114 See reverse 1 con sing of every dileter Sec. 7 cuarse 3 runs in the caches! かんらびれ willand; enel 100 ' 15" sign this is a small creek that ditch; that shalpun culvert saint inty on south eid of rd. Start of birger to dilla die \$MBUMOS Pipeline start 26 78 - 26/25 edry users Drainage CIET MOH Tenyled 5.1017 11164 5-10 Ft Hillor E. 10H CAME TO STO Seg Map Number Parent Materials C. R. C. J. LO III. IN GILLOS hilster dith ditch dith ditt Area ž 418 ×5× 7.5 > > Crown Yes ナ and the of Crown Crown cromu mslope Crown Crown YIDIM 416407 12. , se The CK FOLIAINO TO OLIMAN 12. છું , MARING ٠. ķ 15 .5/ 500, 350'. 400, ,500, ,007 250' 220' 8 11 8 AU V e I Slight to recy shift ed* beof very slight שפנונמום Yery Slight Characteristics 511911 51.9ht slight Use Segment Type 43/10 Con. edos III. Vita. T VEC + ROCK ACTOR 164 160 some 120 Road 응 Sen. edolsino 100,4-4,00/ 100% 100% 100% 100% %8% unded ing 50% 41% 100% 75% eda's esering Road Position 7/46 ێ . ق . . TUIO DEM C.R. O. P. 3. C.P. ن. ت C.R. C. P. Total 3 N 7 3 i 9 3 WAU

rd. surface rd. surface rd. within 5 tt. of south side of rd. ditching on

×

71:

net.

W)

۲

Form 2. Road Segments Draining to Flowing Streams

| Ro | ad Crossing N | pipiline | Stream Type | |
|--------------|-----------------|---|--|------------------|
| √ √ . | | Sketch the Road /Sti (Include only portion directi | ream Configuration y draining to the stream) | |
| ich ///// | * | open and | * * * * * * * * * * * * * * * * * * * | 111111111 |
| | | ROAD | | |
| | Turing | approx 100 ft length Staning water | EN WATER | |
| | | | 1 | |
| | • | Segment 1 | Seg 2 (If needed) | Seg 3 (If needed |
| | Surfacing Type | | / | |
| | Depth of Lift | | | |
| (| Cutslope Veg % | | | |
| | Fillslope Veg % | | | |
| | Ditch Condition | | | |
| | Road Age | | | |
| - | Length | | | |
| | Width | | | |
| | Configuration | | | |
| | Expected Use | | | |
| مهن ليده | Commans | | | |
| | Conmany | | | · |
| _ | | i | 1 | 1 |

Form 2. Road Segments Draining to Flowing Streams

| ноад | Crossing | Number | pipeline | Stream | m Type | • |
|-------------|--------------|-------------|--|--|---|--|
| | | Sketc | h the Road | /Stream Config | uration | |
| | | (Include (| only portion di | rectly draining to | the stream) | |
| il ditch | | | Juliagener 100 Juliagener 100 Tunning Sustantial Tunning Sustan | 100 ft. Experience of the state | this area here offered the to the to the to the to the to the to the | this statem be fairly new would typiain to would typiain to had prevent directly into the water with the towns of the town |
| | L | | | | | |
| | | | Segment 1 | Seg 2 (If | needed) / S | eg 3 (If needed) |
| Sur | facing Type | e | | \(\frac{1}{3} \) | | |
| | Depth of Lif | t | | | | |
| | lope Veg % | I | | | | |
| | slope Veg % | | | | | |
| Ditc | h Condition | | | | | |
| | Road Age | | | | | |
| | Length | | | | | |
| | Width | | | | | |
| | onfiguration | 1 | | | | |
| | pected Use | l l | | | | |
| طعتنا | YE SHOW | | | | | |
| | Common | | | | | |
| F | | | • | | | |
| TOTAL | SEDIMENT | - | | | | |

rm bb-3. Road Erosion Worksheet TOLT WATERSHED

Stossel Cr Rd

ad Segment:

2.38 EDe 9 EDe + 0.95 0.95 0.95 0.95 0.95 0.95 0.95 Armor Factor 0.95 (14) Armor X 2.50 ⊀ 2.50 ₹ 2.50 Y 2.50 Y 2.50 \ 2.50 2.50 2.50 EB*0.05 (13) Vatue 1.80 1.80 8. 8. 1.80 8. 08. 8 8 (12) EFe + 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 Factor $\widehat{\Xi}$ 100 100 100 100 100 100 8 100 100 € % EB.0.20 10.00 10.00 9.0 8.0 10.00 10.00 10.00 10.00 10.00 10.00 (9) Vatue 3.60 3.60 0.00 3.60 3.60 3.60 3.60 3.60 8 EC + 8 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 Factor CUTSLOPE 8 100 8 8 901 80 8 2 No cut No cut 20.00 20.00 EB•0.40 20.00 20.00 20.00 20.00 20.00 20.00 20.00 Rate-EB (4) Basic Erosion S 20 20 S ೪ 20 20 8 Slossel Cr Rock 3 Alluvium lal Segment Length (ft) (2) Road Age 2 b-basin: 0 gment/ (1) Road Site

| | | <u> </u> | | | | 1 | 1 | ı | ₹. | ١. | 1 | t | 1 | ł | | • |
|--------------------|-----------|----------------|---------|---------|-------------|--------|--------|--------|--------|--------|------------|--------|--------|--------|--------|----------------------------|
| | • | (33) | Road | Prism | Acres | 0.289 | 0.757 | 2.183 | 0.029 | 0.138 | 0.138 | 0.138 | 0.103 | 0.052 | 0.23 | |
| | | (32) | Road | Prism | Width/ft | 8 | 35 | 8 | 25 | ೫ | æ | æ | 8 | ೫ | 25 | seoment |
| | | (31) | Segment | Length | = | 420 | 942 | 3170 | SS | 902 | 8 2 | 200 | 150 | 75 | 400 | Total sediment from seamen |
| | ING | (9 | ER | L Eh | Traffic | 18 | 82 | 0 | 22 | 13 | 13 | 13 | 3 | 25 | 10 | Total codi |
| ; | GAMING | (67) | ER | Heavy | Traffic | 128 | 146 | 0 | 179 | 91 | 16 | 91 | 18 | 183 | 82 | |
| | | | | | | | | | | | | | | | | |
| | | (38) | Hazard | Rating | HMA | Σ | MIT | ٦ | = | ¥ | Σ | ¥ | Ĺ | H | M | |
| = ER | | (27) | Overall | ER Rate | 1/ac/yr | 128 | 146 | 0 | 179 | 16 | 91 | 91 | 18 | 183 | 82 | 747 |
| x ERd | ir Y | (92) | | ERd | | 0.7 | 9.8 | 0.0 | 1.0 | 0.5 | 0.5 | 0.5 | 0.1 | 1.0 | 0.5 | |
| | DELIVERY | (23) | Direct | Entry | 26/100 | 6.0 | 9.0 | 0 | 1 | 0.5 | 0.5 | 0.5 | 0 | 1 | 0.4 | nent FR |
| | | (24) | Buffer | Factor | 0 I Z | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.1 | 0 | 0.1 | Total Seement FR = |
| = ERe | | (23) | | ERe | | 183 | 183 | 183 | 179 | . 183 | 183 | 183 | 183 | 183 | 179 | |
| | O | (22) | | ETec | | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | 175.00 | |
| | TRAFFIC | (21) | O.Se | Factor | | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | |
| = ETec) | | (20) | Road | Ose | | Н | Н | Н | Н | Н | Н | Н | Н | н | н | |
| (ETe x Use = ETec) | | (19) | | ETe | | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | |
| - | SURFACING | (18) | | Surface | Factor | 0.2 | 0.2 | 0.7 | 0.2 | 0.2 | 0.7 | 0.2 | 0.2 | 0.2 | 0.2 | |
| | | (11) | Value | ET | B.0.35 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | 17.50 | |

| - | | | | _ | | | | | _ | | | | | | |
|--------|------------------|---------|----------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-----------------------------|
| | (M) | Road | Sediment | tons/yr | 37 | 111 | 0 | \$ | 13 | 13 | 13 | 2 | 6 | 19 | 122 |
| | (33) | Road | Prism | Acres | 0.289 | 0.757 | 2.183 | 0.029 | 0.138 | 0.138 | 0.138 | 0.103 | 0.052 | 0.23 | |
| | (32) | Road | Prism | Width/ft | 30 | 35 | 30 | 25 | 0E | 30 | 30 | 30 | 30 | 25 | segment |
| | (31) | Segment | Length | E | 420 | 942 | 3170 | 80 | 200 | 200 | 200 | 150 | 75 | 400 | Total sediment from segment |
| ING | (06) | ER | Lgh. | Traffic | 18 | 20 | 0 | 77 | £1 | 13 | 13 | 3 | 25 | 10 | Total sedi |
| GAMING | (62) | ER | Heavy | Traffic | 128 | 146 | 0 | 179 | 16 | 16 | 16 | 18 | 183 | 82 | |
| | | | | | | | | | | | | | | | - |

Rebuilt section of upper Stossel Cr road
Stossel Creek Form bb-3. Road Erosion Worksheet

4700 Total Segment Length: Road Segment: Sub-basin:

| EDe + | | 35 | 9 | , | ED. | 3 | ٤ | 3 | | 3 6 | 8 6 | 8 6 | 00 | 00 |
|-----------------------|-----------|------|---------|----------|----------|----------|---------------|--------------|-------------|--------------|-----|-----|-----|-----|
| | DITCH | | 3 | Amor | Pactor | | | | | | | | | |
| | ة | | ? | V V | Š | <u>.</u> | z | z | | | | | | |
| | | (13) | ?: - | Value | Œ | EB*0.05 | 3 | 2 8 8 | 200 | 3 5 | 00 | 0.0 | 0.0 | 0.0 |
| EFe + | | 15 | 3 | | EFe | | e | 0.0 | 00 | 00 | 0.0 | 0.0 | 0.0 | 0.0 |
| | OPE | (| : | Vee | Factor | | ٥ | 0 | | | | | | |
| | FILISLOPE | | | | Vcg. | | : | | | | | | | |
| | | 6 | ? | Value | 53 | EB*0.20 | 22.0 | 22.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| + 23:3 | | (8) | | | ర్జి | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | OPE | ε | } | 8° 2° | Factor | | 0 | 0 | | | | | | |
| | CUTSLOPE | | | | Vcg | - 1 | : | <u> </u> | | | | | | |
| | | ତ | ` | Value | ည္ဆ | EB*0.40 | | 44.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 3 | | (2) | | Basic | Erosion | Rate-EB | 110 | 110 | | | | | | |
| = | | (3) | . ' | Rock | Type | | Reces outwith | Reces outwah | End of spur | road segment | | | | |
| | | 3 | | Koad | Age | ξĹ | | 1 | 1 | | | | | |
| rotal Segment Length: | | ε | • | Koad | Segment/ | Site | 11 | 12 | 13 | | | | | |

| | | 147 | | 0 | Sediment | | ጽ | ~ | 9 | , | 7 | 0 | 6 | 6 | • | 0 | 62 |
|--------------------|------------|------|---------|---------|----------|---------|------|----------|-----|-----|----|-----|-----|-----|----------|----------|-----------------------------|
| | | L | | | | J | 2 | 0.0 | 90 | 2 9 | 2 | 0.0 | 00 | 9 | | 2. | |
| | | | | DEON | | 2 | _ | 15 0 | ١ | | 4 | _ | | | <u> </u> | 4 | |
| | | (45) | | | BEN I | A IGINA | | _ | | | | | | | | | egment |
| | | | (1) | T and h | | ł | 300 | 81 | | Ī | | | | | Ī | | Total sediment from segment |
| | UNC | 99 | 100 | 1 | Tagill | | 8 | 121 | 0 | | > | 0 | 0 | 9 | | * | Total sedin |
| | GAMING | (29 |) E | Teen. | Traffic | VOV | 8 | 1161 | 0 | ٦ | | 0 | 0 | 6 | ٩ | À | |
| | | | | | | .,- | | | | | | | | | | | |
| | | (28) | Hazard | Ratine | HWA | 2 | E : | H | | | | | | | | | |
| = ER | | (2) | Overall | FR Rate | 1/20/vr | Ş | 3 | 121 | 0 | 6 | | 0 | • | 0 | 9 | | 8 |
| x ERd | ار لالم | 93 | | ERd | | Ě | 3 | <u>:</u> | 0.0 | 6 | | 3.0 | 0.0 | 0.0 | 00 | I | _ |
| | DELIVERY | (25) | Direct | Entry | %/100 | ٥ | , | 7 | 0 | | | | | | | | nent ER = |
| · . | | (24) | Buffer | Factor | 2 | 0.0 | | 0 | | | | | | | | | Total Segment ER = |
| = ERe | | (23) | | ERe | | 121 | | 171 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | | |
| | ပ | (22) | | ETec | | 115.5 | 1166 | CC | 0:0 | 0.0 | 5 | 3 | 0.0 | 0.0 | 0.0 | | |
| | TRAFFIC | (21) | Š | Factor | | ~ | | 7 | | | | | | | | | |
| = ETec) | | (20) | Road | O.S. | | | | | | | | | | | | | |
| (ETe x Use = ETec) | | (61) | | ETe | | 23.1 | 22.1 | 1:07 | 0.0 | 0.0 | 6 | | 0.0 | 0.0 | 0.0 | | |
| - 13 | SURFACING | (18) | | Surface | Factor | 9.0 | 70 | 23 | | | | | | | | | |
| | | (1) | Value | EI | EB*0.35 | 38.5 | 38.5 | | 0.0 | 0.0 | 00 | | O'O | 0.0 | 0.0 | | |

Form 1. Road Segments Paralleling Streams Within 200 Ft.

| WAU | Tolt | River | |) | Segment | Type _ | 6 H | | | Se | g Map | Seg Map Number | "\ | 23-24 | Rd | ₹ |
|--------|-----------------|--------|-----------|--------|---------------------------|----------------------|-------------|----------------|------------|-------|------------|-----------------|--------------|---------------------------|------------------------|-------------------|
| Road P | Position | mic | M10-Low | , 5000 | 26 | Use | H | | | Pa | rent N | Parent Material | 7/14 | & OUTWASH | | 50005 6100 ELS |
| | | | | Road | | Characterist | ristics | | | | Area | а | | Drainage | | |
| | | | | | Ì | % | | 7 | -50 | | | | | | | |
| | 13 | ed x x | | | | | 3 | Ino | <u>z</u> . | 72, | 10/ | | \ \ | ed4 | s) | |
| | 100 | 83 | | , o | 1.00 | U_ | | 10 | 4,0 | 410 | eine | | \ Y , | We | U SU | |
| \ | Cen | | SANG TING | SIL | | | UIII BOD | TION THE SUMME | 4 | 1400 | Allo Sinos | | No. TON LIES | | زنون | |
| | CR | ق | 100% | 100% | 166. | >3 | very slight | 420 | 15 | | 765 | | 70%. | ry. Allens | | |
| 7 | <i>U.R.</i> | . , | %00/ | 100% | 169. | _ | 51.948 | 345 | /5 | | 425 | Cread. | 80% | no cross directory | rom eut bar | |
| 3 | C.R. | ذ | %% | 1,00/ | rock | | | .6 mik | 15 | | Ş | | 0% | then too to four sturm | -forther | |
| | | | | | | | | → | | | | | | 174 111 50 | 1/1 rd. low grad | int |
| * | C.R. | ; | \ | 100% | 70ch' Armor | | Slight | 50 | 15 | | 7 | 11.50 11.50 | | | 1/ | |
| | ر. ر | : 3 | | · | mone | | કોંગુરા | . 2 mile | 15 | | | | | 11 # RELIES | CULVEAT | _n |
| N | C.R. | ڻ | 85% | %,90/ | rock Armor | | ships to | 200 | 91 | CLOWN | ٠ | _ | 50% | • | | |
| | C.A. | . 7 | %001 | 100% | Tech Nome | | Slight | 200 | /5 | | 30 | 1/305 | 50% | of Stillin | turines to sulsu to 11 | |
| 7 | C, R. | ٥ ″ | 100% | 100% | VEQ. | | S light | 200 | 15 | CROWN | >- | dikk S | 50% | | ŀ | · \ |
| | 0.0 | · . | | | Tock | | Slight | . ym.lı | 15 | | | | | 111 (. 4 mile | () # REC | in onts |
| 8 | C.R. | e. | 1001 | 100% | 160 | | 31.946 | 150 | 15 | Chow | 80 | dilla t | 50% | 71 | from sputm | |
| 6 | C.R. | و. | 95% | 1,00/ | rock nom | , | 110/2 | 7.5 | 15 | Chown | 7 | | | diated chains | 3 | V. |
| | 6.8 | , 1 | | | · | | Slight | ,25ml | 15 | | | | | 11 (.25 mile) | 7 | ROLL FOR T |
| 0/: | 6.8 | . 9 | / | 100% | rret. | \rightarrow | very digl | 150 | 15 | 15000 | 100% | | _ | ₹ 21 | 16. A.11. | |
| | 0.8 | -hZ 9 | j | 1 | . CP 84 1/ 2/ 2/ | | 418.19 | .9 m | 15 | | | | | Tichely gended | 1 2.4. Sent | مودين فا |
| 71 | | 2.4 | , | 1 | של ב- קנש ום נ | ر چه بران عاملالم | Swite soft | 5 ;ie | - | | 7.15 | ditches | WH. | Kiz culved almost full- A | nost full- A | most comphilli |
| 13 | ~ | 2-4. | 1 | 1 | 2002 | | ý | → | 1 | • | | | | 413-end of spur rd. sogne | ur ra. sogme | J |
| | | | | | · | • | | | | | | | | | | |
| | | | | | | | | | | | | | - | | | |
| Total | al | | | | | | | | | | | 1 | \dashv | | | |

751260 John

Franch

orm bb-3. Road Erosion Worksheet TOLT WATERSHED and Segment: 6170 Rd Stossel-Index Creeks loop bb-basin: Stossel Cr

otal Sc

| ı | _ | | | | _ | | | | _ | _ | | | | | | | |
|----------------------|-----------|--------------|-------|---------|---------|--------------|---------------|---------------|---------------|---------------|------------|------------|------------|------------|------------|------------|------------|
| EDe + | | (10) | | EDe | | 0.0 | 2.4 | 7.7 | 7.7 | 7.7 | 71 | 1.4 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 |
| | CH | (13) | Armor | Factor | | 0 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| | DITCH | (14) | Armon | ኟ | | : | Υ | Y | γ | Υ | Y | γ | Y | Y | γ | Y | Y |
| | | (E1) | Value | 8 | EB*0.05 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5. Y | Y 2.1 | 1.5 Y | 3.0 Y | 3.0 Y | 3.0 Y | 3.0 | 3.0 Y |
| EFe + | | (12) | | EFe | | 1.8 | 1.8 | 1.8 | 3.7 | 1.8 | 1.1 | 1.1 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| | OPE | (11) | Vcg | Factor | | 0.18 | 0.18 | 0.18 | 0.37 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| | FILLSLOPE | (10) | 86 | Vcg | | 80 | 8 | 8 | 20 | 80 | 88 | 80 | 100 | 100 | 80 | 100 | 100 |
| | | (6) | Value | 된 | EB*0.20 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 0.9 | 0.9 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |
| ECe + | | (8) | | స్టి | | 0.0 | 3.6 | 3.6 | 0.0 | 0.0 | 7.6 | 2.2 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |
| |)PE | (<i>a</i>) | Veg | Factor | | 0 | 0.18 | 0.18 | 0 | 0 | 0.63 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| | CUTSLOPE | (9) | 86 | Veg | | : | 80 | 80 | *** | : | 20 | 80 | 100 | 100 | 100 | 100 | 100 |
| | | (5) | Value | ည္သ | EB*0.40 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 12.0 | 12.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 |
| 16900 | | (4) | Basic | Erosion | Rate-EB | SO | 20 | 20 | 20 | 20 | 39 | 30 | 99 | 99 | 3 | 09 | 99 |
| ä | | (3) | Rock | Type | | Reces outwsh | Reces outwith | Reces outwith | Reces outwish | Reces outwith | Vol/sed rx | Vol/sed rx | Ice margin |
| otal Segment Length: | | (2) | Road | Age | yrs | >3 | >3 | >3 | >3 | >3 | >3 | 7 >3 | >3 | >3 | | >3 | >3 |
| otal Segm | | Ξ | Road | egment/ | Site | - | 2 | 3 | Þ | \$ | E< 9 | 7 | 8 | 6 | 10 >3 | 11 >3 | 12 |

| | | (34) | Road | Sediment | tons/yr | 1 | 0 | 0 | 4 | 1 | 12 | 0 | 2 | \$ | 4 | 12 | 21 | 63 |
|---|--------|------|---------|----------|----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|---------------------------------------|-----|------|------------------------------------|
| • | | (33) | Road | Prism | Acres | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.4 | 0.3 | 0.1 | 0.1 | 0.1 | 0.2 | 9'0 | |
| | | (35) | Road | Prism | Width/ft | 20 | 30 | 30 | 25 | 25 | 35 | 25 | 30 | 30 | 30 | 35 | 25 | segment |
| | | (31) | Segment | Length | ະ | 100 | 51 | 100 | 200 | 100 | 200 | 200 | 188 | 150 | 100 | 300 | 1000 | Fotal sediment from segment |
| | ING | (06) | ER | Light | Traffic | 67 | 0 | 0 | 33 | 70 | 18 | 0 | 38 | 15 | 51 | 51 | 36 | Total sedi |
| | GAMING | (62) | 띪 | Heavy | Traffic | 187 | 0 | 0 | 282 | 111 | 220 | 0 | 301 | 439 | 429 | 459 | 301 | |
| • | | | | | | | - | | | | | | | | · · · · · · · · · · · · · · · · · · · | | | |
| | | (88) | Hazard | Rating | HMIL | _1 | 7 | ٦, | د | ٦ | ٦ | د | ب | ר | 7 | ٦ | 7 | ے. |
| i | | (23) | Overall | 3R Rate | Vac/yr | 52 | 0 | 0 | 33 | 20 | 31 | 0 | % | 51 | 51 | 51 | 36 | 9 |

| | GAN | (67) | ER | Heavy | Traffic | 281 | 0 | 0 | 282 | 111 | 220 | 0 | 301 | 429 | 429 | 429 | 301 | |
|--------------------|-----------|------|---------|---------|--------------|------|------|------|------|------|------|------------|------------|------|------|------|------|------------------|
| | | | | - | | | | | | | | | | | | | | • |
| | | (87) | Hazard | Rating | HVMJL | T | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 1 | ٦. |
| ER | | (22) | Overall | ER Rate | t/ac/yr | 29 | 0 | 0 | 33 | 70 | 16 | 0 | 9 C | 15 | ıs | 15 | ж | 9 |
| x ERd | RY | (97) | | ERd | | 0.8 | 0.0 | 0.0 | 8.0 | 5.0 | 1.0 | 0.0 | 2.0 | 1.0 | 1.0 | 1.0 | 0.7 | |
| • | DELIVERY | (22) | Direct | Entry | 26/100 | 0.8 | 0 | 0 | 8.0 | 0.5 | 1 | 0 | 0.7 | 1 | 1 | 1 | 1 | nent ER |
| | | (24) | Buffer | Factor | 0 = X | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Total Segment ER |
| = ERe | | (23) | | ERe | | 37 | 43 | 43 | 41 | 39 | 31 | 97 | 51 | 51 | 15 | 51 | 51 | |
| | ၁ | (22) | | ETec | | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | 21.0 | 21.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | |
| | TRAFFIC | (21) | Ç | Factor | | \$ | 2 | \$ | 5 | \$ | \$ | 5 | 5 | \$ | \$ | \$ | \$ | |
| (ETe x Use = ETec) | | (20) | Road | Use | | L | L | L | J | L | L | L | L | ı | 7 | 7 | 1 | |
| (ETe x Us | | (61) | | ETe | | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.2 | 4.2 | 8.4 | .8.4 | 8.4 | 8.4 | 8.4 | |
| | SURFACING | (18) | - | Surface | Factor | 0.4 | 0.4 | 9.4 | 0.4 | 0.4 | 1.0 | 6.4 | 4.0 | 9.4 | 0.4 | 9.4 | 0.4 | |
| | | (17) | Value | 百 | EB*0.35 | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | 10.5 | 10.5 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | |

STOSSEL Cl. Form 3. Road Segments With Erosion Indicators Seg Map 6100 SPIR Segment Type 3.2 mi WAU TOUT Position OUTWASH PLAN Use 6 6 (L) Indicator Surface Type KG Surf. Depth 4-6 Road Age > 3 Parent Material GLACIAL RIVER GRAVEL FUTURE OF STATE OF THE PROPERTY OF THE PROPERT Configuration Direct Entry? Filsopered Comments 44PE Width Ditch SHEAM ENTRY OUSE FILL SOT NONE 100' OUT MOSPY 90 + GRASS POTIOLES 2190-4 007 PORD BTWN 2-3 NO 3-4 RELIEFCULUSLIS J OUT NO DRAIN CUT A DITTIL ONLY RODO OUTSLOPED 50+ VEG- PUTY ROTS ZOO' Major Strem XING LG ROCK ON FILL 12 CULVERS SURFACE RO MOSTLY FITTER THOUGH FILL Royd UEG ENTRY OUSE FILL- TO SOON TRESCH SUI 6+17 5% 100' Gusss RUIS 10% 5-30 80+ 500 RELIEF CULVER, do of sinem percent PSOUL ON SLOPE RILLS 5001 80+80+ 61055 151 LUEL FLUME ON CULUSET 600 GNASS MUS 1001 100 most by my mitter THROUGH GARSS ON MULE \$ DITTHES

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Total

TOLT WATERSHED

bb-3. Road Erosion Worksheet
Segment: F35 and F30
asin: Lower N.Fork/Yellow Cr.

0.0 2.2 (12) EFe + 0.18 0.08 0.18 Factor 95 (10) % Veg 0.37 8 8 EB*0.20 0.0 0.0 0.0 (9) Value EF 4.3 1.4 0.0 0.0 0.0 0.0 ථු EC + € (3) Veg Factor 0.18 0.18 8 8 ⊙ % % § No cat 24.0 No cut 20.0 50/5 24.0 24.0 12.0 (5) Value EC EB*0.40 0.0 0.0 (4) Basic Erosion Rate-EB 888 श्र Reces outwish Rock Type Undif drift Vol/sed rx Kame Segment Length: (2) Road Age nd ent/

2.4 0.0 0.0

0.95

2.5 Y

0.0

0.0 0.0

1.5

0.0

0.0

0.95

0.95

3.0 ₹ 3.0

EDe

Armor Factor

(14) Armon Y/N

(13) Value ED

EB*0.05 3.0

(95)

EDe +

| -2- | | (83) | Hazard | Rating | HMML | M | 7 | Н | M | M | | | |
|--------------------|-----------|------|---------|---------|--------------|-------|-------|-------|-------|-------|-----|-----|-----|
| # ER | | (27) | Overall | ER Rate | t/ac/yr | 149 | 77 | 218 | 601 | 144 | 0. | 0 | 0 |
| x ERd | RY | (92) | | ERd | | 0.7 | 0.1 | 1.0 | 1.0 | 8.0 | 0.0 | 0.0 | 00 |
| • | DELIVERY | (22) | Direct | Entry | 26/100 | 0.7 | 0 | 1 | - | 0 | | | |
| | | (24) | Buffer | Factor | 0 = Z | 0 | 0.1 | 0 | 0 | 9.0 | | | |
| = ERe | | (23) | | ERe | | 212 | 215 | 218 | 109 | 181 | 0 | 0 | C |
| | င | (22) | | ETec | | 210.0 | 210.0 | 210.0 | 105.0 | 175.0 | 0.0 | 0.0 | 0.0 |
| | TRAFFIC | (21) | Cse | Factor | | 0\$ | 20 | 20 | 20 | 20 | | | |
| (ETe x Use = ETec) | | (20) | Road | Use | | Н | H | н | Н | H | | | |
| (ETe x Us | | (61) | | ETe | | 4.2 | 4.2 | 4.2 | 2.1 | 3.5 | 0.0 | 0.0 | 0.0 |
| | SURFACING | (18) | | Surface | Factor | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | | |
| | | (11) | Value | ET | EB*0.35 | 21.0 | 21.0 | 21.0 | 10.5 | 17.5 | 0.0 | 0.0 | 0.0 |

| | , | _ | | | _ | | _ | _ | _ | _ | | _ | a . |
|--------|------|---------|--------|----------|-----|-----|-----|-----|-------------|-----|-----|-----|-----------------------------|
| | (34) | Road | •• | tons/yr | 20 | * | 09 | 6 | 88 | 0 | 0 | 0 | 152 |
| | (33) | Road | Prism | Acres | 1.0 | 0.2 | 0.3 | 0.1 | 0.4 | 0.0 | 0.0 | 0.0 | |
| | (32) | Road | Prism | Width/ft | 30 | 30 | 30 | 30 | SE | | | | segment |
| | (31) | Segment | Length | z | 200 | 300 | 007 | 115 | 9 9 9 | | | | Total sediment from segment |
| NC | (30) | ER | Light | Traffic | 16 | 3 | 29 | 15 | 18 | 0 | 0 | 0 | Total sedi |
| CAMING | (62) | ER | Heavy | Traffic | 149 | 22 | 218 | 109 | 144 | 0 | 0 | 0 | |
| | | | | | | | | | | | | | _ |

#5-5m2>

Form 1. Road Segments Paralleling Streams Within 200 Ft.

| | ÿ | | | | | | <u>ن کور</u> کور | . S. S. | 114) | 30.00 | | | _ | | | | | | | | | |
|-------------------------------|-------------------|-----------------|--------|--|--------|---------------------|---------------------|----------------------------|---------------|---|---|---|---|---|----------|---|---|---|--|--|---|-------|
| + F50 9E sictions 29,20,21 | G1901AL - VOL/560 | Drainage | | Suel Wax W Viet | inos | 496 claps to write; | ور مل مرا مرود | large gre 1 Fillipse mound | To be seed to | حرار در کورز و درود کوست بدر درارد کورز و درود کوست بد | | | | | | | | | | | | |
| F55 + F50 26~ 86 81 | 1.9614 | Drai | | 1 | 4 | * | à Z | | | | | | | | | | | | | | | · |
| mber | | | 2 | Ten | II. | | 7514- | dilch Homs into | 2 F.4. A. | re 10 . 18 ft | | | | | | | | | | | | |
| Seg Map Number | Parent Material | Area | | \ . | • / | fill clop | Picos | | 10Md swime | f. Uslope | | | | | | | | | | | | |
| Seg N | Paren | 1 | | 12. | OJJUO | m 710 | 011 | 3/6 3/8 | 34 415 | Occ 350/ | | | | | | | | | | | | |
| | Ξ1 | | | / | 14 | + | | 15' Crown 10 | 15. autoba | 20' putition | | | | | | | | | | | | |
| | 7 27 | | OUINI | 130 | Eio, | 200' 1' | | | 1/2. /: | 500' 20 | | | | | | | | | | | | |
| 6 H | MAINLINE | Istics | SOUNT! | 10 | CUINA | rery slight 20 | | 2/4 | | 12 Slight 50 | , | | | | | | | | | | | |
| nt Type | - Use | Characteristics | % | \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ | POR I | | | (,, | | | · | | | | | | | | | | | |
| Segment | | Road (| | 507.00 507.00 | Os III | 70.4 200 | 3% may 19 | 316 tommend (700ck norm | 60% 200 | 95% TOCK | | _ | | | | | | | | | | |
| | PURIN | | | Consolitation (Consolitation) | Olesko | 7 | / | 0, 200/ | | | | | | | | | | | | | | |
| | 7111 P | 1 | 90 | \$ \\ \frac{1}{2} | ins | \ : | , | Ø | ٥/ | £3,0 <i>y</i> | - | | | | - | | _ | _ | | | | |
| | i | | | 47.00 | eins. | R. 6 | و | ٥ | 9 | <i>و</i> ز د | | | | | | _ | _ | | | | _ | |
| 764 | Position | | | 14100 | dem | 1 C.R. | 0.5 | 0.5 | 0.5 | 0.8 | | | • | - | \dashv | | - | - | | | - | lal |
| WAU | Road | | | | | | 7 | <u>n</u> | 20 4 | 52. | | | | | | | | | | | | Total |

#1 grand been them road grading present along both sides of 1d.

original rutland auch appears to have been derained (?) / receded to the point of small erect. Howing thru-unable to locate culvert - apparently water submerging a resurbaing on other side of rawy.

old culverts found (shotgun style) now located approx. 50 tt. Away from curant-water source-(to the) emptied into severely gowing stream old (now day),

MAY LLUW SErsonary TO A CLOSED DEPRESSION

#3 whire south edge of rd. is bermed w/ rd. surfacing material - 0% slope

rm bb-3. Road Erosion Worksheet

TOLT WATERSHED

ad Segment: Mainline 80 from T70 to Dry Cr

Lower S.Fork and Upper N. Fork

Site gment/ Road (E tal Segment Length(ft): b-basin: 4 >3 3 >3 >3 >3 Age yrs (2) Road Reces outwsh Reces outwsh Reces outwish Reces outwsh Reces outwsh Alluvial fan Reces outwish Rock Type Erosion Rate-EB (4) Basic S 50 SO S 50 EB*0.40 (5) Value EC 20.0 ---20.0 20.0 20.0 ---20.0 ---20.0 ---Veg. % 3 8 2 Factor **ç** 3 0.18 0.18 ECe + Š **®** 3.6 8 3.6 8 0.0 0.0 EB*0.20 Value (9) 10.0 10.0 10.0 10.0 10.0 10.0 % <u>(</u> TLLSLOPE 8 8 8 S 50 SO Factor (11) Veg 0.18 0.18 0.37 0.63 0.37 EFe + (12) EFe 3.7 ... 1.8 1.8 EB*0.05 (13) Value ED 2.5 7 2.5 Y 2.5 Y 2.5 N 2.5 Y 2.5 Armor Y/N Ξ Factor Armor (15) 0.95 0.95 <u>0.9</u>5 EDe + EDe <u>(16</u> 2 2 25 25 2.4 2.5

| | õ | $\overline{}$ | T. | <u> </u> | F | Ĕ | , | | <u></u> | | - - | | | 1 |
|--------------------|-------|---------------|-------|----------|-------|-------|--------------|-------|---------|---------|----------------|------|-----------|-------------------|
| | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | 17.5 | EB*0.35 | ET | Value | (17) | | |
| | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | Factor | Surface | | (18) | SURFACING | |
| | 3.5 H | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | | ETe | | (19) | | (ETex U |
| | H | Н | H | Ξ | I | H | Н | Н | | Use | Road | (20) | | ETe x Use = ETec) |
| | 50 | 50 | 50 | 50 | S0 | 50 | 50 | 50 | | Factor | Use | (21) | TRAFFIC | |
| | 175.0 | 175.0 | 175.0 | 175.0 | 175.0 | 175.0 | 175.0 | 175.0 | | ETec | | (22) | С | |
| | 197 | 184 | 183 | 183 | 181 | 179 | 181 | 181 | | ERe | | (23) | | = ERe |
| 77. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | N = 0 | Factor | Buffer | (24) | | |
| Palal Casmani ED = | _ | 1 | 1 | 1 | 1 | 1 | 1 | _ | %/100 | Entry | Direct | (25) | DELIVERY | |
| ' | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | ERd | | (26) | RY | x ERd |
| 30 | 197 | 184 | 183 | 183 | 181 | 179 | 181 | 181 | t/ac/yr | ER Rate | Overall | (27) | | ER |
| _ | Ξ | I | H | I | Ξ | Ξ | Ξ | Ξ | H/M/L | Rating | Hazard | (28) | | |

| 388 | | segment | Total sediment from segment | Total sedi | |
|----------|-------|----------|-----------------------------|------------|---------|
| 11 | 0.1 | 25 | 100 | 39 | 197 |
| 25 | 0.1 | 30 | 200 | 26 | 184 |
| 59 | 0.3 | 35 | 400 | 25 | 183 |
| 101 | 0.6 | 30 | 800 | 25 | . 183 |
| 36 | 0.1 | 25 | 250 | 24 | 181 |
| 31 | 0.2 | 25 | 300 | 22 | 179 |
| 31 | 0.2 | 25 | 300 | 24 | 181 |
| 104 | 0.6 | 25 | 1000 | 24 | 181 |
| tons/yr | Acres | Width/ft | = | Traffic | Traffic |
| Sediment | Prism | Prism | Length | Light | Heavy |
| Road | Road | Road | Segment | ER | ER |
| (£) | (33) | (32) | (31) | (36) | (29) |
| | | | | ING | GAMING |
| | | | • | | |

8

to swam or row Cont Cont

Form 1. Road Segments Paraneling Streams Within 200 Ft.

2-26-83

609 .0 3, BILLO WAU Road Position Total Ø Ś 1 ω Was Poling 7017 0.5 ر. د: 0 0.5. 0.S. 0.5 0.S 0.5. Surace Type can provide) Stretch this Fielict you + 2 708 SIOPE 112 Ç 120 Sur. Depth The map that Kigarding. this was alm to too Gou will notice b area had froblemo with stides.

It's pure familian with the area and 120 10% 80% 00: Cuislobe. Veg fully. Intermation. 25% 25% 5000 50% 10033 Ş 100% 100% (Tills 10 De. Ved - of ACLUVIACUSE Road Characteristics Segment Type __ Continued , and luch with 7001 . 1104 100x.0 Suem F SIGN CH Armor Ø Dich Some crossings were not whitten S Pool Age much snow Slight Shehl slight 70 Sighl 3 20 RURING OF GUILBING HEBUY I MUCK Main LINE 00. 1900/ 300/1 800 FL 300/2 250 ft. 8 1000/1 length .42 24. 125. ۲. įÿ ۲۲. Ċ Wides Slope I with proderymo inslok (10st) outstoped Crownia חשלם בינננו Configuration Por Seg Map Number Maidiae from TH. 60 - to Dry com Parent Material × <u>۲</u>۰۲ 27.5 ×2, ž Area Direct Entry? ditth dilch rd. surfou dilch rd Inc rd. sul Palhuay 1-211. 511. 4/4. How Para Ro = Rzeessional Stream Type Drainage ALCUVIAL created when road clieria occurring on w side. H. crosion says rd. flowing down into river signs of high crosion + gul unable to determine scening soft. Not hinge de 12 snow; fillsto Connents ロッアンナメエ assing; direct entry 50 SO fing food side? material bern te rates, of wow -y whire 11.(11) 0661111 arity or 1 con 1.3. gui.

8,0

rm bb-3. Road Erosion Worksheet
ad Segment: Mainline 60 road
b-basin: Lower S. Fork

TOLT WATERSHED

| ıal Segn | lal Segment Length: | . | 20500 | | | | ECe + | | | | EFe + | | | | EDe + |
|----------|---------------------|--------------|---------|---------|-------------|--------|-------|---------|-----------|--------|-------|---------|----------|--------|-------|
| | | | | | CUTSLOPE |)PE | | | FILLSLOPE | OPE | | | DITCH | 요 | |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) |
| Road | Road | Rock | Basic | Value | | Veg. | | Value | 8 | Veg | | Value | Armor | Armor | |
| gment/ | Age | Туре | Erosion | EC | Veg. | Factor | ECe | EF | Vcg | Factor | EFe | E | ¥ | Factor | EDe |
| Site | ya | | Rate-EB | EB*0.40 | | | | EB*0.20 | | | | EB*0.05 | | | |
| - | >3 | Reces outwsh | SO | 20.0 | 20.0 no cut | 0 | 0.0 | 10.0 | 100 | 0.18 | 1.8 | 2.5 | Υ | 0.95 | 2.4 |
| 2 | 2 >3 | Reces outwsh | 50 | 20.0 | 20.0 no cut | 0 | 0.0 | 10.0 | 90 | 0.18 | 1.8 | 2.5 | Υ | 0.95 | 2.4 |
| 3 | >3 | Reces outwsh | 50 | 20.0 | 20.0 no cut | 0 | 0.0 | 10.0 | 85 | 0.18 | 1.8 | 2.5 | Υ | 0.95 | 2.4 |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| - | - | | | | | - | | | | | | | | | |

| ٦ | 21 | 10 | Total Segment ER = | Total Seg | | | | | | | |
|----------|---------|-------|--------------------|-----------|-------|-------|---------|-------------------|-----------|-----------|---------|
| | ြ | 0.0 | | | o | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| z | 143 | 0.8 | 0 | 0.8 | 179 | 175.0 | 50 | Н | 3.5 H | 0.2 | 17.5 |
| X | 111 | 0.6 | 0.6 | 0.05 | 179 | 175.0 | 50 | H | 3.5 H | 0.2 | 17.5 |
| Ξ | 179 | 1.0 | 1 | 0 | 179 | 175.0 | 50 | H | 3.5 | 0.2 | 17.5 |
| HIM/L | t/ac/yr | | %/100 | Z = 0 | | | | | | Factor | EB*0.35 |
| Rating | ER Rate | ERd | Entry | Factor | ERe | ETec | Factor | Use | ETe | Surface | 띡 |
| Hazard | Overall | | Direct | Buffer | | | Use | Road | | | Value |
| (28) | (27) | (26) | (25) | (24) | (23) | (22) | (21) | (20) | (19) | (18) | (17) |
| | | RY | DELIVERY | | | C | TRAFFIC | | | SURFACING | |
| | = ER | x ERd | | | = ERe | | | ETe x Use = ETec) | (ETe x Us | | |

| 207 | 1.4 | . 30 | | 17 | 143 |
|----------|-------|----------|---------|---------|---------|
| 27 | 0.2 | 30 | 350 | 13 | 111 |
| 95 | _ | 30 | 450 | 22 | 179 |
| tons/yr | Acres | Width/ft | = | Traffic | Traffic |
| Sediment | Prism | Prism | | Light | Heavy |
| Road | Road | Road | Segment | ER | ER |
| (34) | (33) | (32) | (31) | (36) | (29) |
| | , | | | ING | GAMING |

Total sediment from segment

0.0 0.0 0.0

10,500 Tt - Mae WHEEL

Form 1. Road Segments Paralleling Streams Within 200 Ft.

eal. Out W WAU **Road Position** Total W N Map Poin, 7014 0.5 0.S. *0.*s. Surace Type 714 ; e, ë Sur. Depth Cursiope. Ved & 90% 85% 100% Cillstope. Led % Road Segment Type Armar Armar VEB. Characteristics Use Post Age Slight slight moderate Rusing or Gullynon E H 210016 35011 4501 length اکن 15' 204 Width Crown Crown UNION Configuration Parent Material Seg Map Number 70 715 776 Area Oirect Entry? diteh+ なべな Pathway How Rary RECESSIONA 26×86 Stream Type Drainage Concrete bridge; 0-4/a (sout) wite endy 4:

N' sate of and desirt entry wise the K. Africa ?5

tong channel entrief from and of delik is the outviet in war mon - a migor Sict. - 23, 26, 35. 36 . some brewer Connents MAILLINE OUTW ASH -Doninase Shope vize side endge die

9 90 12

orm bb-3. Road Erosion Worksheet
oad Segment: 60 Rd 26N8E S23
ub-basin: Yellow Cr

TOLT WATERSHED

| ub-basin: | | Yellow Cr | | | | | | | | | | ′ | | | | |
|-----------|----------------------|---------------|-----------|-------------------|----------|--------|-------|---------|-------------|--------|---------|---------|----------|---------|---------|------|
| otal Segn | otal Segment Length: | # | 9500 | | | | ECe + | | | | EFe + | | | | EDe + | |
| | | | | | CUTSLOPE |)PE | | | FILLSLOPE | OPE | | | DITCH | | | |
| (E) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | <u>E</u> | (15) | (16) | |
| Road | Road | Rock | Basic | Value | % | Veg. | | Value | 88 | Vcg. | | Value | Armor | Armor | | |
| egment/ | Age | Туре | Erosion | EC | Vcg. | Factor | ECe | 甲 | \c <u>g</u> | Factor | EFe | B | ž | Factor | EDe | |
| | yra | | Rate-EB | EB*0.40 | | | | EB*0.20 | | | | EB*0.05 | | | | |
| 1 | >3 | Reces outwish | SO | 20.0 | 75 | 0.37 | 7.4 | 10.0 | 80 | 0.18 | 1.8 | 2.5 | Υ | 0.95 | 2.4 | |
| 2 | >3 | Reces outwsh | 50 | 20.0 | 100 | 0.18 | 3.6 | 10.0 | 80 | 0.18 | 1.8 | 2.5 | Υ | 0.95 | 2.4 | |
| u | >3 | Reces outwish | SO | 20.0 | 100 | 0.18 | 3.6 | 10.0 | 80 | 0.18 | 1.8 | 2.5 | Y | 0.95 | 2.4 | |
| ۸ | >3 | Till/vol rx | 40 | 16.0 | SO | 0.37 | 5.9 | 8.0 | 80 | 0.18 | 1.4 | 2.0 | Z | 1 | 2.0 | |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | |
| | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | |
| | | | (ETe x Us | ETe x Use = ETec) | | | = ERe | • | | x ERd | ■ ER | | | | | |
| | | SURFACING | | | TRAFFIC | С | | | DELIVERY | RY | | | , | GAMING | NG | |
| | (17) | (18) | (19) | (20) | (21) | (22) | (23) | (24) | (25) | (26) | (27) | (82) | | (29) | (30) | (31 |
| | Value | | | Road | Use | | | Buffer | Direct | | Overall | Hazard | | EX | | Segm |
| | ET | Surface | ETe | Use | Factor | ETec | ERe | Factor | Entry | ERd | ER Rate | Rating | | Heavy | Light | Leng |
| | EB*0.35 | Factor | | | | | | Z = 0 | %/100 | | t/ac/yr | H/M/L | | Traffic | Traffic | = |
| 1 | 17.5 | 0.2 | 3.5 | T | 5 | 17.5 | 29 | 0 | | 1.0 | 29 | Ļ | | 187 | 29 | |
| 2 | • 17.5 | 0.2 | 3.5 | L | 5 | 17.5 | 25 | 0 | 1 | 1.0 | 25 | L | | 183 | 25 | |
| u | 17.5 | 0.2 | 3.5 | L | 5 | 17.5 | 25 | 0 | 1 | 1.0 | 25 | L | | 183 | 25 | |
| 4 | 14.0 | 0.2 | 2.8 | L | 5 | 14.0 | 23 | 0 | 0 | 0.0 | 0 | L | | 0 | 0 | 21 |
| | 0.0 | | 0.0 | | | 0.0 | 0 | | | 0.0 | 0 | | | 0 | 0 | |
| | 0.0 | | 0.0 | | | 0.0 | 0 | | | 0.0 | 0 | | | 0 | 0 | |
| | 0.0 | | 0.0 | | | 0.0 | 0 | | | 0.0 | 0 | | | 0 | 0 | |
| | 0.0 | | 0.0 | | | 0.0 | ٥ | | | 0.0 | 0 | | | 0 | 0 | |

| ≅ | | segment | Total sediment from segment | Total sedi | |
|----------------|-------|----------|-----------------------------|------------|---------|
| 0 | 0.0 | | | 0 | 0 |
| 0 | 0.0 | | | 0 | 0 |
| 0 | 0.0 | | | 0 | 0 |
| 0 | 0.0 | | | 0 | 0 |
| 0 | 1.4 | 30 | 2100 | 0 | 0 |
| 8 | 0.3 | . 35 | 400 | 25 | 183 |
| 8 | 0.3 | 35 | 400 | 25 | 183 |
| 2 | 0.1 | 35 | 75 | 29 | 187 |
| tons/yr | Acres | Width/ft | Į, | Traffic | Traffic |
| Sediment | Prism | Prism | Length | Light | Heavy |
| Road | Road | Road | Segment | ER | ER |
| (X | (33) | (32) | (31) | (30) | (29) |
| | | | | ING | CAMING |

Total Segment ER =

9

45 pt 2,00 ובא עוד טכ WAU Road Position Total Map Point P Surface Type 7 Tor 5 76" 6 6 : Sur. Depth 5 35.5 100 75% S Cursione. Veg % 100 7 80+ 80+ 80 508 80+138en Cills lode. Yed % Road Segment Type + Bean Characteristics 6 a Use S (J w 1 W Post Age S116H 2000 WASHOO LIGHT Rusing or Gullying 7 400' 00/4 100, Ø length. 400 15 15 3 3 Wideh CENER OCLOW 700 007 187 Configuration E Parent Material Seg Map Number 7 7 Area Olfect Entry? Fill ゴビ X PARRIAN イント ,5 W w GLACIAL OUTWASH Hon Sara 8 SITE AM TAPE Drainage 0 XING 5.60. t ? XIIG 770 GARDE -アノハンア 4 ガル Connents 9 ŧ ESOCIAL- PL 3 12% 6 100 NBOR ۶ ۲ 8600 HX3 OSFIM 1500 ROCK - Corrying 127% CC 100€ 130 3 6 73S 71NG or accor 0000 0.4

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Comer semon

> 5 5

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1. 8 mil

Form bb-3. Road Erosion Worksheet

TOLT WATERSHED

Total Road Segment: Sub-basin: Lower S. Fork T70 mainline rd to reservoir

| Total sediment from segment | ment fro | Total sedi | | ľ | ٦ | 2 | н | Total Segment ER = | Total Segi | | | | | į | | | |
|-----------------------------|----------|------------|---------|-----------------|---------|---------|--------|--------------------|------------|-------|------------|----------|-------------------|---------|-----------|-----------------------|------------|
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | - |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| 20 | 1000 | 2 | 18 | سد | L | 18 | 0.1 | 7 | 0.1 | 181 | 175.0 | SO | H | 3.5 | 0.2 | 17.5 | _ |
| | n, | Traffic | Traffic | | HM/L | t/ac/yr | | %/100 | N = 0 | | | | | | Factor | EB*0.35 | |
| Prism | Length | Light | Heavy | | Rating | ER Rate | ERd | Entry | Factor | ERe | ETec | Factor | Use | ETe | Surface | ET | |
| _ | Segment | ER | ER | الاست. حينيا | Hazard | Overall | | Direct | Buffer | | | Use | Road | | | Value | |
| (32) | (31) | (30) | (29) | | (28) | (27) | (26) | (25) | (24) | (23) | (22) | (21) | (20) | (19) | (18) | (17) | |
| | | ING | GAMING | | | | RΥ | DELIVERY | | | C | TRAFFIC | | | SURFACING | | |
| | • | | | | | = ER | x ERd | | | = ERe | | | ETe x Use = ETec) | | | | |
| | £ | | | | | | | | | | | | | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| | | 2.5 | _ | Z | 2.5 | 0.0 | 0 | -0- | 10.0 | 3.6 | 0.18 | 80 | 20.0 | 50 | Moraine | >3 | |
| | | | | | EB*0.05 | | | | EB*0.20 | | | | EB*0.40 | Rate-EB | | YT3 | Site |
| | | · EDe | Factor | ¥ | ED | EFe | Factor | Vcg . | EF | ECe | Factor | Veg. | EC | Erosion | Type | Age | Segment/ |
| | | | Armor | Armor | Value | | Veg | | Value | | Vcg | % | Value | Basic | Rock | Road | Road |
| | | (16) | (15) | (14) | (13) | (12) | (11) | (01) | 9 | 8 | 9 | 9 | (5) | 3 | (3) | 2 | Ξ |
| | | | CH | DITCH | | | ,OPE | FILLSLOPE | | | OPE | CUTSLOPE | | | | | |
| | • | EDe + | | | | EFe + | | | | ECe + | | | | 7400 | # | Total Segment Length: | Total Segn |

(32) Road Prism Width/ft

Road (33)

(34) Road

Acres

lons/yr

8 8 8 8

88

Prism Sediment

Form 1. Road Segments Paralleling Streams Within 200 Ft.

| WAU | E I | 704 | 7 | | Se | Segment Type | Туре _ | 6 H | | · | Sec | д Мар | g Map Number | | 7 | 70 - | 7838 | 125870: V |
|------|--------|--------|------------------|-------------|------|--------------|----------------|---------|----------|--------|-------|---------------|--------------|------------------|----------|------------|-----------|-----------|
| Road | | S /~ | TOR B | BENCH | | | Use | 16 Н | エ | | Pal | rent Material | terial | | MORANE | | <u>``</u> | 7 3 |
| | | | | | Road | | Characteristic | istics | | | | Area | ש | 0 | Drainage | Ф | \ | |
| | | 14 | 4 | BIA | . \ | ES T | 9 | 2 | Guisinos | 70, | | tion | 215 | | 100 | 200 | Ġ | |
| | 4 | Mad Su | Surface Surf. | Sur. Cursic | 1 26 | 10 | Dich Ro | RURIT | | lenon. | Widek | Confidur | Palhy | 164 YOU | 1.67 | COMA | COMM | |
| | | Rb- | 6"+ | 80+ | 80+ | 8000 | >3 | 534 | 1.4m | 20' | CK | ∠ - | 1 | | 100 | -0NG-6 | | 1 |
| | | | | | | | | | | | | | | | 5,72 | B1724 - NO | 100 | è è |
| | | | | | | | | | | | | | | | BU | BLADED. | 3 | 1 |
| - | · | | | | | | | | | | | | | | 1212 | 1 | 0.500 | 7000 |
| | | | | | | | | | | | | | | | 77 | ness | -wo | 2 |
| | | | | | | | | | | | | | | | ans | 1 | Down of | ari |
| | | | | | | | | | | | | | | | Smare | 1 | Gucis | 30 2 |
| | | | | | | | | | | | | | | | Spuz | • | ROAD | K |
| | - | - | | | | | _ | | | | ļ | 1 | - | | D1771 | | ERODING | アノダ |
| | - | 26 | 6"+ | | | | (A) | GNLLIES | | | | 1.~ | | 1 | RIGHT | ı | Ross E | 7 3003 |
| | | | | | | 2000 | <u> </u> | | | | | <u> </u> | | | 800 | Eroons | 0, | .533 |
| | | | | | | | | | | | | _ | • | | Co/m | 5/4 | 0 5 | 250, |
| | | | | | | | | | | | | | | | DIRN | 7. | 9 | 7. 4. |
| | | | <u> </u> | | | | | | | | | | | | Deans | | | wer/ |
| | | | _ | | | | <u> </u> , | | | | | <u> </u> | | | 3 case | | 23012 | ٥٢ ٢٥ |
| _ | | | | | | | | | | | | | | | Saire | ľ | SME | • |
| | | | | | | | - | | | _ | | - | | \vdash | | | | |
| | Total | | | | | | | | | | | | | | | | | |

| Controlled Con | | 0.0 | | 0 | 0 | 0 | سبت | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
|--|------------------|-------|----------|---------|---------|---------|------------|---------|---------------|--------|--------|---------|-------------|------------|--------|-----------|------------------|----------------|------------|----------|
| Color Worksheet Color Work | | 0.0 | | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| Color Workshed Colo | | 0.0 | | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0.0 | | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0.0 | | | 0 | 0 | | | 0 | 0.0 | , | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| The contain worksheet The | | 0.0 | | | 0 | 0 | | | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 | |
| | | 0.1 | 30 | 100 | 27 | 185 | | L | 27 | 1.0 | 1 | 0 | 27 | 17.5 | 5 | [| 3.5 | 0.2 | 17.5 | 2 |
| | | 0.1 | 25 | 250 | 2.4 | 181 | | 7 | 24 | 1.0 | | 0 | 24 | 17.5 | 5 | L | _ | 0.2 | 17.5 | _ |
| Color Colo | tons/ | Acres | Width/ft | = | Traffic | Traffic | | 1-I/M/L | t/ac/yr | | %/100 | N = 0 | | | | | | Factor | EB*0.35 | |
| Color Worksheet Figure | _ | Prism | Prism | Length | | Heavy | | Rating | ER Rate | ERd | Entry | Factor | ERe | ETec | Factor | Use | ETe | Surface | ET | |
| Color Colo | Road | Road | Road | Segment | | ER | | Hazard | Overall | | Direct | Buffer | | | Use | Road | | | Value | |
| Control Cont | (2) | (33) | (32) | (31) | (36) | (29) | لب. | (28) | (27) | (26) | (25) | (24) | (23) | (23) | (21) | (20) | (19) | (18) | (13) | |
| Red Position Worksheet FOLT WATERSHED Coltrolled Position Worksheet Position Worksheet Position Worksheet Position Worksheet Position | | | | | C | GAM | 1 | | | NY | DELIVE | | | C | TRAFF | | | SURFACING | | |
| Color Worksheet FOLT WATERISHED | | | | • | | | _ | | ■ ER | x ERd | | | = ERe | | | : = ETec) | (ETex Us | | | |
| Color Colo | | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Note Foreign Found Foreign Found Foreign Found | | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Note Figure Fig | | | | | 0.0 | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Figure F | | | | | 0.0 | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Figure F | | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Figure F | | | | | 0.0 | | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 | | | | |
| Fig. | | | | | 2.4 | 0.95 | | 2.5 | 3.7 | 0.37 | 50 | 10.0 | 3.6 | 0.18 | 100 | 20.0 | 50 | Alluvial fan | >3 | 2 |
| Fig. Food | | | | | 2.4 | 0.95 | _ | 2.5 | 3.7 | 0.37 | 50 | 10.0 | 0.0 | 0 | | | 50 | Reces outwsh | >3 | _ |
| Cold Waltersheel TOLI Walter | | | | | | | | EB*0.05 | | | | EB*0.20 | | | | EB*0.40 | Rate-EB | | yra | Site |
| Road Brosion Worksheet FOLT WATERSHED | | | | | EDe | Factor | ¥ | ED | EFe | Factor | Veg. | ᄠ | S E | Factor | ٧cg | BC | Erosion | Туре | Age | ment/ |
| . Road Erosion Worksheet TOLT WATERSHED | | | | | | Armor | Armor | Value | | Veg | % | Value | | ٧ ٠ | 98 | Value | Basic | Rock | Road | oad |
| . Road Erosion Worksheet IOLT WATERSHED sent: 90 Rd 26N9E SE1/4 7 Upper N. Fork sent Length(II): 3200 ECe + FILLSLOPE DITCH CUTSLOPE FILLSLOPE | | | | | (16) | (15) | (<u>•</u> | (13) | (12) | (II) | (10) | (9) | (8) | (7) | 6 | (5) | (4) | (3) | (2) | Ξ |
| . Road Brosion Worksheet TOLT WATERSHED sent: 90 Rd 26N9E SE1/47 Upper N. Fork ent Leneth(t): 3200 ECc + EFc + | | | | | | | DIT | | | | FILLSL | | | 1 | CUTSLO | | | *** | o | |
| . Road Erosion Worksheet sent: 90 Rd 26N9E SE1/47 Upper N. Fork | | | , | | EDe + | | | | 11 10 + | | | | + 2 3 | | | | 3200 | | ent Leneth | al Seen |
| ad Erosion Worksheet | | | | | | | | | | | 5 | | | | | | | Upper N. Fork | | o-basin: |
| | | | | | | | | | | | | | | Ü | LEKSH | IOLI WA | 7 | osion Workshee | . Koad Er | T 00-3 |

⊙ ′

Segment/ Total Segment Length(ft): Sub-basin: Road Segment: Form bb-3. Road Erosion Worksheet (1) Road EB*0.35 Value ET (2) Road 3 Age ă 8 8 0.0 8 8 Reces outwsh Upper N. Fork 90 Rd 26N9E SE1/4 7 Reces outwsh SURFACING Surface Factor (81) Rock Type 0.2 0.2 (ETe x Use = ETec) Erosion Rate-EB Basic ETe (19) 140 3 8888 3.5 G 0.0 8 3.5 S 50 G TOLT WATERSHED EB*0.40 Road Value EC U_{3e} (20) 20.0 0.0 99 8 0.0 0.0 Factor CUTSLOPE (21) U**se** RAFFIC ٧eg % 3 ಜ Factor ETec €3 (22) 0.37 0.0 8 0.0 <u>بر</u> 35 ECe + = ERc ERe (2) S E **®** 0.0 8 8 0.0 8 90 20 (9) Value EF Factor Total Segment ER = EB*0.20 Buffer Z I O (24) 00000 0.0 8 Entry %/100 Direct DELIVERY Veg \mathfrak{Z} FILLSLOPE % (<u>i</u> 0 8 Factor x ERd ERd **(3**) **cg** (11) 0.63 8 0.0 88 8 99 5 5 EFe + ER Rate Overall (23) (12) (/ac/yr EFe ER 8 9 0:0 9 8 9 చ 8 (28) Hazard HM/L Rating EB*0.05 (13) Value ED 0.0 0.0 0.0 0.0 8 Armor Y/N ≺ (<u>F</u> DITCH Armor Factor Heavy (15) Traffic (29) Ę GAMING 0.95 0.95 191 188 0 0 EDe + Total sediment from segment Traffic Light EDe (16) 면 (Se 0.0 9 0.0 0.0 Segment Length (31) \$ 300 Width/ft Prism (32) Road ଞ ષ્ઠ Prism Road Acres (33) 0.0 8 0.0 8 8 8 0.3 0.2 Sediment tons/yr (34) Road

4 WAU Road Position Total 1 Map Polh, 66 2 7017 0.5 0.5 0.5 Surrace Type ACLUVIAC Ċ 111 1400 Sur. Depth 50% Cuisione. Ved % 65% 1000 Form 1. 50% imm 75% 50% 20% Fillslope, Led % Road Characteristics Segment Type 13 W. W. TOCK TOCK Road Segments Paralleling Streams Within 200 Ft. \$05K + 76:1 Use Post Ade Dicor or . Snow 335 ? Snow commeds sous - c RURING OF GUILANDS 77 1 250 300 400. 100. 7 length 9 15. व् 5, 18 Wides outstay of Stope et t Serve Crowner Configuration Parent Material Seg Map Number Rd 7.4 705 35 Area Direct Entry? ditch, ditch 36 PARKWAY Com 1178 74. 26 N 9E -How Rary 3- RECESS. 60 70 ASH Stream Type 4. 90 Drainage advised striky Deceasing on S.

3-441 Stoped to the of returned

Tel. beginning to the E state my
Sin beginning to the first of the

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The stope SE W 7 ted completely woshed out Connents のりか たりり in their so - NEC15 Tight to asset ! side of ed; 0,7%

Form bb-3. Road Erosion Worksheet Road Segment: F20 Rd

TOLT WATERSHED

Total Segment Length: Sub-basin: Segment/ Site Road (2) Road Age Reces outwsh Lower S. Fork Rock Erosion Rate-EB Basic 7200 3 EB*0.40 (5) Value EC 20.0 8888 þ % 3 ខ Factor **6** 3 ECe + S E 8 0.00 8 8 99 8 EB*0.20 Value 퍉 ૭ 10.0 10.0 000000 0.0 % 🤶 Factor **g**(Ξ 0.53 0.63 Ele + EFe (12) 2000 8 0.0 EB*0.05 (13) Value ED 00000 00 2.5 -0-Armor Y/N Ξ Factor Armor (15) 0.95 EDe + (16) 00 00 ခြ 99 0.0

| Color Colo | | _ | | _ | _ | _ | _ | _ | ~ | _ | | | - | ~ | 1 |
|--|----------------------|---------|---------|-----------|-------|---------|---------|-------|-----------|---------|------------------|---------------|----------------|-----------|-----------|
| CTe x Use = ETec TRAFFIC TRAF | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 17.5 | 17.5 | EB*0.35 | ET | Value | (17) | | |
| TRAFFIC (21) (22) (23) (24) (25) (25) (26) (27) (28) (29) (21) (21) (22) (23) (24) (25) (25) (26) (27) (27) (27) (27) (27) (27) (27) (27 | | | | | | | | 0.2 | 0.2 | Factor | Surface | | (18) | SURFACING | |
| TRAFFIC (21) (22) (23) (24) (25) (25) (26) (27) (28) (29) (21) (21) (22) (23) (24) (25) (25) (26) (27) (27) (27) (27) (27) (27) (27) (27 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.5 | 3.5 | | ETe | | (19) | | (ETe x Us |
| C DELIVERY ERd ER (22) | | | | | | | | Ĺ | 7 | | Use | Road | (20) | | e = ETec) |
| ### RERE | | | | | | | | 5 | 5 | | Factor | Use | (21) | TRAFFI | |
| X ERd | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 17.5 | 17.5 | | ETec | | (22) | С | |
| ERd = ER (Y) (26) (27) Overall ERd ER Rate Use/yr 0.8 24 0.1 2 0.0 0 0 0 0 0 0 1 | | | | | | _ | | | _ | _ | - | | _ | | נ |
| ERd = ER (Y) (26) (27) Overall ERd ER Rate Use/yr 0.8 24 0.1 2 0.0 0 0 0 0 0 0 1 | | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 30 | | ERe | | (23) | | = ERe |
| ERd = ER (Y) (26) (27) Overall ERd ER Rate Use/yr 0.8 24 0.1 2 0.0 0 0 0 0 0 0 1 | Total Seg | 0 | 0 | 0 | 0 | 0 | 0 | | 30 0 | Z = 0 | | | - | | = ERe |
| | Total Segment ER | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | _ | Factor | Buffer | (24) | DELIVE | = ERe |
| (28) Hazard Rating H/M/L L | Total Segment ER = | 0.0 | 0.0 | 0 0.0 | 0.0 | 0.0 | 0 0.0 | 0.1 0 | 0 0.8 | _ | Factor Entry | Buffer | (24) (25) | DELIVERY | |
| | Total Segment ER = 1 | 0.0 0.0 | 0 0.0 0 | 0 . 0.0 0 | 0.0 0 | 0 0.0 0 | 0 0.0 0 | 0.1 0 | 0 0.8 0.8 | %/100 | Factor Entry ERd | Buffer Direct | (24) (25) (26) | DELIVERY | x ERd |

| 0 | 0 | 0 | 0 | 0 | 0 | 18 | 150 | Traffic | Heavy | ER | (29) | DNIMVD | |
|-----|-----|-----|-----|-----|-----|-----|-----|----------|----------|---------|------------------|--------|--|
| 0 | 0 | 0 | 0 | 0 | 0 | 2 | 24 | Traffic | Light | ER | (36) | ING | |
| | | | | | | 125 | 175 | [; | Length | Segment | (31) | | |
| | | | | | | 15 | 20 | Width/ft | Prism | Road | (32) | | |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | Acres | Prism | Road | (33) | | |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | tons/yr | Sediment | Road | (£) | | |

Total sediment from segment

Road Segment: Form bb-3. Road Erosion Worksheet TOLT WATERSHED

Lower S. Fork

F20 Rd abandoned portion to Lynch Lk

Total Segment Length: Sub-basin: Segment/ Road (2) Road Age Reces outwsh Rock Type (4) Basic Erosion Rate-EB 2000 EB*0.40 (5) Value EC 0.0000000 CUTSLOPE ۷cg % 3 ઝ Factor **2** 3 0.53 ECe + EC 8 8 8 8 200 0.0 EB*0.20 Value EF 00 00 00 0.0 10.0 -0-% (<u>c</u> Factor **&** (E) EFe+ 퍉 (12) 0.0 0.0 99 99 00 EB*0.05 (13) Value ED 2000 9.0 99 0.0 2.5 -0-Armor Y/N (] DITCH Armor Factor (15) EDe + EDe (16) 88 8 0000 0.0 8

| - | 9 | H | nent ER | Total Segment ER = | | | | | | ! | |
|--------|---------|-------|----------|--------------------|-------|------|---------|--------------------|-----------|-----------|---------|
| | 0 | 0.0 | | | ြ | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| | 0 | 0.0 | | | 0 | 0.0 | | | 0.0 | | 0.0 |
| 1 | 12 | 1.0 | | 0 | 12 | 1.8 | 0.1 | Z | 17.5 | -1 | 17.5 |
| H/M/L | l/ac/yr | | %/100 | N = 0 | | | | | | Factor | EB*0.35 |
| Rating | ER Rate | ERd | Entry | Factor | ERe | ETec | Factor | Use | ETe | Surface | 四 |
| Hazard | Overall | | Direct | Buffer | | | Use | Road | | | Value |
| (28) | (27) | (26) | (25) | (24) | (23) | (22) | (21) | (20) | (19) | (18) | (17) |
| | | RY | DELIVERY | | | C | TRAFFIC | | | SURFACING | |
| | · ER | x ERd | | | = ERe | | | (ETe x Use = ETec) | (ETe x Us | | |

| GAMING | ING | | | | |
|---------|---------|---------|----------|-------|----------|
| (29) | (36) | (31) | (32) | (33) | (34) |
| ER | ER | Segment | Road | Road | Road |
| Heavy | Light | Length | Prism | Prism | Sediment |
| Traffic | Traffic | 7 | Width/ft | Acres | tons/yr |
| 886 | 98 | 1500 | 12 | 0.4 | 5 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |
| 0 | 0 | | | 0.0 | 0 |

Total sediment from segment

Form 3. Road Segments With Erosion Indicators WAU TOLT Seg Map F20 Segment Type LYNCH CLEEK Road
Position Bevery Use ABNONES Indicator _____ Surface Type Road Age 334 Parent Material Kane Des RIVER GRENZE 1.3 mi Ruthing of Chitying Contiguration Direct Entry? SHESTI TYPE Fillstope, ved Confinents Width Ditch 12" 0% LEVEL STREOM DIVERTO DOWN RO 1~10 ADDO CATEGORES 7 SEE ATTOCHED SHECT # 10-20 SEE ATTACKSO SHEET #2 2 0-290 1251 2050 RILLS LEVEL ROAD PARAURES 5 Mison W/IN 20-30' FOR 125-1 SUEF. SLASH ON SLOPE & SUBNT GREANL-BEEM PREVENT MUCH SSOIMENT OLLIUSMY Total

Form 2. Road Segments Draining to Flowing Streams

| Road Crossing N | Sketch the Road /S | | |
|-----------------|----------------------------|----------------------------|----------------------------------|
| · · | include only portion direc | tly draining to the stream |) |
| | Auston | / FZO DO | ↑ |
| H. | 93 WEST W | THE LYNCH | LYNCH LAKE |
| | نظر خراد ان الم | ١ ٧ | STREAM CULVET |
| | | ₩. D | eta Has Fromso |
| | | Fic | OUS IN AND OUT OF MAN DEPRESSION |
| | | | NE WASHED OUT. |
| | Segment 1 | Seg 2 (If needed) | Seg 3 (If needed) |
| Surfacing Type | RIVE GROVEL | | |
| Depth of Lift | 0-2 | | |
| Cutslope Veg % | 20 - 50 | | |
| Fillslope Veg % | NO FILLS | | |
| Ditch Condition | NOT FUNCTIONING | 15-THELE | |
| Road Age | 73 yrs | | |
| Length | ~ 1500 | | |
| Width | 12-15-1 | | |
| Configuration | LEVEL-CONV | E¥ | |
| Expected Use | ABRNDONED | 7 | |
| Gerain | 0 % | | |
| Common | | OLUSET WATER ST | TILL Froms COUN RO |
| | AT PEAK From | | |
| | | | |

TOTAL SEDIMENT

Form 2. Road Segments Draining to Flowing Streams

Sketch the Road /Stream Configuration (Include only portion directly draining to the stream)

| 556- 2 | <i>↑</i> _N |
|----------|-----------------------|
| 201gg | |
| FILSCOPE | DIFZH SEG. 1 |
| 50 ft | 275' |
| Ful I | Fill SLOPE. |
| Crusti | CTO AT BANK - ERSOING |

| | Segment 1 | Seg 2 (If needed) | Seg 3 (If needed |
|------------------|----------------|-------------------|------------------|
| Surfacing Type | RIVER Graver | Rover Graver | |
| Depth of Lift | TO 8' AT FILL | | |
| Cutslope Veg % | NO CUTS | 80 t | · . |
| Fillslope Veg % | LITTLE | 20% | |
| Ditch Condition | SOME UEG- | VEG- | |
| Road Age | > 3 4RS. | 73 YRS. | |
| Length | 125 | 50' | |
| Width | 151 | 121 | |
| Configuration | LEVER OR CROWN | LEUSE OR OUT | |
| Expected Use | LIGHT TWCK | GENEUSL | |
| CRACIENT COMPANY | 0-17. | 3-5-76 | |
| Commons | FILL ACROSS | | |
| | CLEEK | | |
| | | | |
| TOTAL SEDIMENT | | | |

TOLT WATERSHED

Form bb-3. Road Erosion Worksheet
Road Segment: 50 Road above dam
Sub-basin: South Fork above dam
Total Segment Length(ft): 11350

| | | | | | | | | | | | | | | | | | Site | Segment | Road | (1) | | Total S |
|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|--|----------------|----------------|----------------|----------------|----------------|---------|---------|---------|---------|--------------|-------|---------|-----------|---------------------------|
| 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 > | 2 > | | |)ii | ۵. | | | egme |
| >3 | >3 | >3 | >3 | >3 | >3 | 2< | >3 | >3 | >3 | >3 | >3 | >3 | >3 | 5< | >3 | >3 | угз | Age | Road | (2) | | Total Segment Length(ft): |
| Alpine glacial | Alpine glacial | Alpine glacial | Alpine glacial | Alpine glacial | Alpine glacial | Moraine | Moraine | Moraine | | Type | Rock | (3) | | <u> </u> |
| SO | 50 | 50 | 50 | SO | SO | S0 | 20 | SO | 8 | SO | 8 | SO | So | 50 | SO | 50 | Rate-EB | Erosion | Basic | 3 | | 11350 |
| 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | EB*0.40 | EC | Value | છ | | |
| īğ | 100 | 18 | 100 | 18 | 18 | 70 | 18 | 100 | 100 | 18 | 70 | 18 | 18 | 100 | 70 | : | | Veg | % | <u></u> | CUTSLOPE | |
| 9.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.37 | 0.18 | 0.18 | 0.18 | 0.18 | 0.37 | 0.18 | 0.18 | 0.18 | 0.37 | 0 | | Factor | Veg | 9 | OPE | |
| 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 7.4 | 3.6 | 3.6 | 3.6 | 3.6 | 7.4 | 3.6 | 3.6 | 3.6 | 7.4 | 0.0 | | ECe | | (8) | | ECe + |
| 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | EB*0.20 | EF | Value | ૭ | | |
| 18 | 18 | 18 | 18 | 100 | 18 | <u>1</u> 8 | 100 | 18 | 18 | 18 | 18 | <u>8</u> | 18 | 2 | 18 | 8 | | Vcg. | 8 | (10) | FILLSLOPE | |
| 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | | Factor | Vcg. | (11) | OPE | |
| 1.8 | | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | | EFe | | (12) | | EFc + |
| | | | | | 2.5 | | | | · 2.5 | 2. | 2. | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | EB*0.05 | ED | Value | (13) | | |
| 2.5 Y | Z | 2.5 Y | 2.5 Y | 2.5 Y | 7 | 2.5 N | 2.5 Y | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | 7 | 2.5 N | 2.5 Y | 2.5 Y | 2.5 Y | 7 | 7 | 7 | | _ | Armor | (£) | DI | |
| 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | 0.95 | 0.95 | 0.95 | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0 | | Y/N . Factor | Armor | (15) | DITCH | |
| 2.4 | 2.4 | 2.4 | | | | 2.5 | | | | 2.5 | 2.4 | 2.4 | 2.4 | 2.4 | 2.4 | 9.0 | | EDe | | (16) | | EDe + |

| | | | (ETe x Us | ETe x Use = ETec) | | | = ERc | | | x ERd | = ER | | | | | • | | | |
|------------|---------|-----------|-----------|-------------------|---------|------|-------|--------|----------|----------|---------|--------|---|---------|---------|---------|----------|------------|----------|
| | | SURFACING | | | TRAFFIC | ì | _ | | DELIVERY | RY | | | | GAMING | NG | | | | |
| | (17) | (18) | (19) | (20) | (21) | (22) | (23) | (24) | (25) | <u>8</u> | (27) | (28) | _ | (29) | (30) | (31) | (32) | (33) | (£ |
| | Value | | | Road | Use | | | Buffer | Direct | | Overall | Hazard | | ER | ER | Segment | Road | Road | Road |
| | ET | Surface | ETe | Use | Factor | ETec | ERe | Factor | Entry | ERd | ER Rate | Rating | | Heavy | Light | Length | Prism | Prism | Sediment |
| | EB*0.35 | Factor | | | | | | N = 0 | %/100 | | 1/ac/yr | HWYL | | Traffic | Traffic | = | Width/ft | Acres | tons/yr |
| _ | 17.5 | 0.2 | 3.5 | C | - | 3.5 | S | 0 | 1 | 1.0 | Ş | - | | 177 | 19 | 225 | 8 | 0.2 | - |
| 2 | 17.5 | 0.2 | 3.5 G | C | - | 3.5 | 15 | 0 | 1 | 1.0 | 15 | | | 187 | 29 | 8 | 36 | 0.3 | 5 |
| دي | 17.5 | 0.2 | 3.5 | C | | 3.5 | 11 | 0 | 1 | 1.0 | 11 | L | | 183 | ય | 470 | છ | 0.3 | 4 |
| _ | 17.5 | 0.2 | 3.5 G | G | 1 | 3.5 | 11 | 0 | 1 | 1.0 | 11 | ٦ | | 183 | z | 150 | ઝ | 0.1 | - |
| v | 17.5 | 0.2 | 3.5 G | G | 1 | 3.5 | 11 | 0.15 | 0.65 | 0.7 | 8 | L | | 128 | 18 | \$ | છ | 0.3 | 2 |
| 6 | 17.5 | 0.2 | 3.5 G | G | 1 | 3.5 | 15 | 0 | - | 1.0 | 15 | | | 187 | 8 | 350 | 8 | 0.2 | |
| 7 | 17.5 | 0.2 | 3.5 | G | 1 | 3.5 | 11 | - | 0 | 1.0 | = | ٢ | | 183 | z | 8 | ષ્ટ્ર | 0.0 | 0.2 |
| 00. | 17.5 | 0.2 | 3.5 G | O | | 3.5 | 11 | 0.2 | 1 | 1.0 | = | ۲ | | 183 | ĸ | 8 | 33 | 0.2 | 3 |
| 9 | 17.5 | 0.2 | 3.5 | G | 1 | 3.5 | 11 | 0 | 1 | 1.0 | = | ٢ | | 183 | 25 | 8 | 35 | <u>0.1</u> | 0.9 |
| 10 | 17.5 | 0.2 | 3.5 | O | 1 | 3.5 | 11 | 0 | 1 | 1.0 | = | | | 183 | 25 | 18 | 36 | <u>0:1</u> | 0.8 |
| | 17.5 | 0.2 | 3.5 | G | 1 | 3.5 | 15 | 0 | 1 | 1.0 | 15 | | | 187 | 29 | 350 | 35 | 0.3 | 4 |
| 12 | 17.5 | 0.2 | 3.5 G | G | 1 | 3.5 | .11 | 0 | 1 | 1.0 | 11 | | | 183 | z | 200 | હ | <u>0.1</u> | 2 |
| 13 | 17.5 | 0.2 | 3.5 G | G | 1 | 3.5 | 11 | 0 | 1 | 1.0 | 11 | L | | 183 | 25 | 18 | 8 | <u>0.1</u> | 0.8 |
| 14 | 17.5 | 0.2 | 3.5 | C | _ | 3.5 | == | 0 | 1 | 1.0 | 11 | L | | 183 | ಜ | 300 | ઝ | 0.2 | 2 |
| <u>ن</u> ۲ | 17.5 | 0.2 | 3.5 | G | _ | 3.5 | = | 0 | 1 | 1.0 | 11 | ١ | | 183 | 25 | 500 | છુ | 0.3 | 4 |
| = : | 17.5 | 0.2 | 3.5 G | G | _ | 3.5 | Ξ | 0 | 2 | 1.0 | 11 | | | 183 | 25 | 300 | 35 | 0.2 | u |
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| | | 0.1 | 30 | 150 | 25 | 183 |
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| | tons/yr | Acres | Width/ft | fi | Traffic | Traffic |
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Form 1. Road Segments Paralleling Streams Within 200 Ft.

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Form 1. Road Segments Paralleling Streams Within 200 Ft. Segment Type Seg Map Number Son Shoot O

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| ₹oad | Road | Rock | Basic | Value | % | Veg | | Value | | Veg | | Value | Armor | Armor | |
| gment/ | Age | Туре | Erosion | EC | Veg | Factor | ECc | 甲 | Vcg | Factor | EFe | ED | ž | Factor | EDe |
| Site | yrs | | Rate-EB | EB*0.40 | | | | EB*0.20 | | | | EB*0.05 | | | |
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| | | SURFACING | | | TRAFFIC | С | | | DELIVE | DELIVERY | | | | GAMING | NG |
| | (17) | (18) | (19) | (20) | (21) | (22) | (23) | (24) | (25) | (26) | (27) | (28) | | (29) | (30) |
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| | EB*0.35 | Factor | 513 | Osc | ractor | 2912 | EKC | N = 0 | %/100 | EKG | EK Kalc t/ac/уг | H/M/L | | Traffic | Traffic |
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| | 21 | 0.2 | 4.2 | G | 1- | 4.2 | 13.53 | 0 | 0.02 | 0.02 | 0.27 | - | | 4.3866 | 0.6066 |
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Form 3. Road Segments With Erosion Indicators

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orm bb-3. Road Erosion Worksheet

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| EDe + | | (16) | | EDe | 2.5 | 2.5 | 2.5 | 3.5 | | ING | (30) ER | Light Traffic | 1.27 | 1.27 | 15.55 | 0 |
|-------|---------------|--------------|-------|--------------------|--------------|----------|--------------|--------------|--------------------|-----------|-----------------|--------------------|-------|-------|-------|--------|
| | Н | (15) | Armor | Factor | 1 | 1 | 1 | 1 | | GAMING | (29) ER | Hcavy Traffic | 9.145 | 9.145 | 94.3 | 0 |
| | DITCH | (14) | Armor | X.X | z | z | z | z | | | | | | | | |
| | | (13) | Value | ED FB*0.05 | | 2.5 | 2.5 | 3.5 | | | (28) Hazard | Rating H/M/L | L | L | J | L |
| EFc + | | (12) | | EFe | 1.8 | 1.8 | 3.7 | 2.52 | = ER | • | (27) Overall | ER Rate 1/ac/yr | 0.71 | 0.41 | 86.9 | 0 |
| - | JOPE | (11) | Veg | Factor | 0.18 | 0.18 | 0.37 | 0.18 | x ERd | 3RY | (26) | ERd | 0.05 | 0.05 | 0.5 | 0 |
| | FILLSLOPE | (01) | % | Vcg | 8 | 8 | 20 | 80 | | DELIVERY | (25) Direct | Entry %/100 | 0.05 | 0.05 | 0 | 0 |
| | | (6) | Value | EF FB*0.20 | 10 | 10 | 10 | 14 | | | (24) Buffer | Factor $N = 0$ | 0 | 0 | 0.5 | 0 |
| EC + | | (8) | | EC _e | 3.6 | 3.6 | 7.4 | 10.36 | = ERe | | (23) | ERe | 14.2 | 8.25 | 13.95 | 21.28 |
| | ISLOPE | (<i>u</i>) | Veg | Factor | 0.18 | 0.18 | 0.37 | 0.37 | | <u>[</u> | (22) | ETcc | 6.3 | 0.35 | 0.35 | 4.9 |
| | CUTSL | (9) | % | Veg | 8 | 8 | 09 | 20 | | TRAFFIC | (21) Use | Factor | 1.8 | 0.1 | 0.1 | 1 |
| | | (s) | Value | EC EB*0.40 | 20 | 20 | 20 | 28 | (ETe x Use = ETec) | | (20) Road | Use | Ð | z | z | ڻ ن |
| | | (4) | Basic | Erosion Rate-EB | 20 | 20 | 20 | 70 | ETe x Us | | (19) | ETc | 3.5 | 3.5 | 3.5 | 4.9 |
| | | (3) | Rock | Type | Reces outwsh | Kame | Reces outwsh | Reces outwsh | | SURFACING | (18) | Surface Factor | 0.5 | 0.5 | 0.5 | 0.2 |
| | | (2) | Road | Age vrs | >3 | >3 | >3 | 2 | | | (17) Value | ET EB*0.35 | 17.5 | 17.5 | 17.5 | 24.5 |
| | | (1) | Road | Segment/ Site | G26N8E29 > 3 | on26827A | 170 non | 183 B | | | | | | | | |

ROADS WORKSHEET B3 TOLT AREA ********** - SEC * ff = FIELD FORM B-2 COLUMN NUMBER 1 2 3 5 6 7 8 --CUTSLOPE--ROAD ROAD ROCK BASIC VEG SEGMENT AGE TYPE RATE VALUE % VEG FACTOR (ff-2)* (ff-4)* (ff-5)* TABLE B-5 (calc)(ff-7)* TABLE B-6 (calc) 6H-26/8-8 29-33-22 _ALLUVIUM 50 20.00 90 0.18 3.60 ÄCLUVIUM 50 20.00 90 0.18 3.60 6H-26/8-C26-33-36 MOD WEATH 30 12.00 90 0.18 2.16 6H-26/9-B31-30-MOD WEATH 30 12.00 90 0.18 2.16 6L-26/8-6-2 7>3 MOD WEATH 30 12.00 90 0.18 2.16 MOD WEATH 30 12.00 90 0.18 2.16 MOD WEATH CEC. 12.00 90 0.18 2.16 NUN26827A >3 MOD WEATH Kan 230 12.00 90 0.18 2.16 TOLT RDADS WORKSHEET B3 AREA ********* 9 10 12 13 15 1€ 11 -FILLSLOPE------DITCH----VEG ARMOURED ARMOUR VALUE % VEG FACTOR VALUE EFe (Y/N) FACTOR EDe (calc) (ff-8)* TABLE B-6 (calc) (calc) (ff-10)* (text) (calc) 10.00 . 90 0.18 1.80 2.50 Ν 1.00 2.50 10.00 90 0.18 1.80 2.50 N 1.00 2.50 1.50 6.00 90 0.18 1.08 N 1.00 1.50

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| | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| | VALUE (calc) | ROAD TYPE | SURFACE FACTOR | ETe | ROAD USE | USE FACTOR TABLE B-9 | : ETer | RATE | |
| | 17.50 17.50 10.50 | | 0.20 | 3.50 3.50 2.10 | | 36.10 36.10 36.10 | 126.35 126.35 75.81 | 134.25 | |
| | 10.50 10.50 10.50 | EL | 0.20 0.20 0.20 | 2.10 | L | 36, 10 | | 90 ES | |
| | | EL EN | 0.20 | 2.10 2.10 | G | | 3.78 | | |
| F | ROADS | WORKSHEET | B3 | TOLT ******* | | 9 (************************************ | | 10 - 20 | • |
| | 25 | 26 | 27 | 28 | | | 31 | | |
| (| ROAD | OUTSLOPE FACTOR | OUTSLOFE ERe | % DIRECT ENTRY (ff-11)* | ERODBLTY ERd (calc) | BUFFER FACTOR (text) | OVERALL EROSION | RATING H/M/L | FIELI CHECKE (Y/N) |
| - | Y Y Y | 0.90 | 120.83 | 0.05 0.05 | 6.04 | 1.00 1.00 1.00 | 6.04 | L | Y Y Y |
| | Y Y Y | 0.90 0.90 0.90 | 72.50 18.44 18.44 | 0.10 0.05 0.05 | 7.25 0.92 0.92 | 1.05 1.00 1.00 | 7.61 0.92 0.92 | L L L | $\begin{pmatrix} z \\ z \end{pmatrix}$ |
| | Y | 0.90 0.90 | 7.67 4.46 | 0.05 0.05 | 0.38 0.22 | 1.00 | 0.38 0.22 | L L | 7 × |
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Form 3. Road Segments With Erosion Indicators

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| Surface | Type | | Su | ırf. Depti | ۱ | R | oad Ag | رe <u>ک</u> | S_ Par | ent | Material. | RECESS OUTH | 13 NA |
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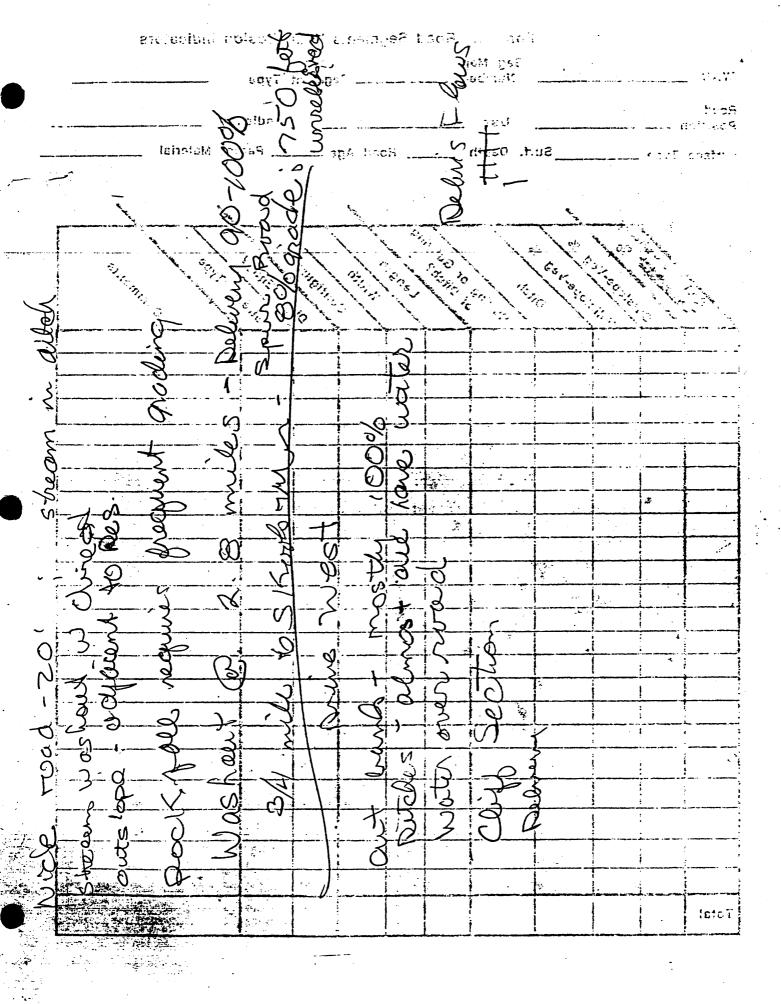
STOSSEC CE Form 3. Road Segments With Erosion Indicators WAU TOCT Seg Map 6183-B Segment Type 26NBE 530-31 0.9 MILES 2-19-93 MZ Ruting of Gulfing Contiguration Direct Entry? ope wey ved of Stream LONG GROW, W/O CULUSITS - RILLIAG ROSO DITCHES CARMING SEAMET Total

Form bb-3. Road Erosion Worksheet

| | | | | | 47 | - | 2.0 | | | 1 |
|----------------------------|-------|-------|-------------|-------|----------|-----------|----------|-----------|--|---|
| | EDe + | | (16) | | EDe | | 2 | | | |
| | | Ŧ | (14) (15) | Armor | Factor | | 1 | | | |
| | | DITC | | | | | Z | | | |
| | | | (13) | Value | ED | EB*0.05 | 2 N | | | |
| | EFe + | | (12) | | EFe | | 3.0 | | | |
| | | LOPE | (10) (11) | Veg | Factor | | 0.37 | | | |
| | | FILLS | (10) | % | Veg |) | 20 | | | |
| | | | (6) | Value | EF | EB*0.20 | 8 | | | |
| | ECe+ | | (8) | | S S | | 5.9 | | | |
| | | OPE. | (8) (1) (9) | Veg | Factor | | 0.37 | | | |
| | | CUTSE | | | | | +09 | | | |
| | | | (5) | Value | EC | EB*0.40 | 16 50 | | | |
| | , | | (4) | Basic | Erosion | Rate-EB 1 | 40 | | | |
| hlands | | | (3) | Rock | Type | | Andesite | | | |
| ads - Hig | | | (2) | | | | >3 | | | |
| Surveyed roads - Highlands | | | (1) | Road | Segment/ | Site | 9F | Reservoir | | |

| | ING | (30) | T is | Traffic | 77 | 0 | 0 |
|---------------------------|---------------|---------------------------|--------------------|--------------|------|---|-----|
| | GAM | (29) (30) | Heave | Traffic | 675 | 0 | 0 |
| | | | | | | | |
| | | (27) (28) | Hazard | HVM/L | Σ | | |
| = ER | | (27) | Overall FR Rate | t/ac/yr | 76.8 | | |
| x ERd | ERY | (56) | FRA | | 0.95 | | |
| | DELIVI | (25) | Putro | %/100 | 0.95 | | |
| | | (23) (24) (25) (26) | Butter | 0 Z | 0 | | |
| | | _ | _ | • | 80.9 | | . * |
| | IC | (22) | FTP | | 70.0 | | |
| (| TRAFF | (21) (22) | Factor | | 5 | | |
| $(ETe \times Use = ETec)$ | | (20) | | | 7 | | |
| (ETe x U | | (61) | H e e | | 14.0 | | |
| | SURFACING | (18) | Surface | | 1 | | |
| | | (17) | Value | EB*0.35 | 14 | | |

| (29) (30) ER ER Heavy Light Traffic Traffic 675 77 0 0 | | | | | | |
|--|-----|------------|------------------|-----|---|---|
| GAN. (29) ER Heavy Traffic 675 0 | | (30) ER | Light Traffic | 11 | 0 | 0 |
| <u> </u> | GAN | (29) ER | Heavy Traffic | 675 | 0 | 0 |



n bb-3. Road Erosion Worksheet

surveyed road systems - Lowlands

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|-------|-----------|--------------|-------|---------|---------|--------------|---|---|---|--------------------|-----------|--------------|---------|--------------------|--------|---|---|---|
| EDe + | | (16) | | EDe | - | 3.5 | 0 | 0 | 0 | | ING | (30) | ER | Light Traffic | 2.45 | 0 | 0 | 0 |
| | - | | • | | | | | | | | GAMING | (29) | ER | Heavy Traffic | 13.475 | 0 | 0 | 0 |
| | DITCH | (14) | Armor | XX | | z | | | | | C | • | | | | | | |
| | | (13) | | ED | EB*0.05 | 3.5 | 0 | 0 | 0 | 5 | | (28) | Hazard | Rating H/M/L | | | | |
| EFe + | | (12) | | EFc | | 7 | 0 | 0 | 0 | = ER | | 11 | Overall | ER Rate t/ac/yr | 1.47 | 0 | 0 | 0 |
| | OPE | (11) | Veg | Factor | | 0.5 | | | | xERd | iry | (26) | • | ERd | 0.05 | 0 | 0 | 0 |
| | FILLSLOPE | (01) | % | Veg | | 0 | | | | | DELIVE | (25) | Direct | Entry %/100 | 0.05 | | | |
| | | 6) | Value | 된 | EB*0.20 | 14 | 0 | 0 | 0 | | | (24) | Buffer | ractor N = 0 | 0 | | | |
| ECe + | | (8) | | EC | | 14 | 0 | 0 | 0 | = ERe | | (23) | | ERc | 29.4 | 0 | 0 | 0 |
| | OPE | (<i>a</i>) | Veg | Factor | | 0.5 | | | | | آ آ | (22) | | ETcc | 4.9 | 0 | 0 | 0 |
| | CUTSL | (9) | | | | 0 | | | | | TRAFFIC | (21) | Cse | Factor | T | | | |
| | | (5) | Value | EC | EB*0.40 | 28 | 0 | 0 | 0 | (ETe x Use = ETec) | | (20) | Road | Use | ව | | | |
| • | | (4) | Basic | Erosion | Rate-EB | 70 | | | | | | (61) | 1 | ETe | 4.9 | 0 | 0 | 0 |
| | | (3) | | | | Reces outwsh | | | | | SURFACING | (18) | | Surface Factor | 0.2 | | | |
| | | (2) | Road | Age | yrs | 2 | | | | | | (17) | Value | ET EB*0.35 | 24.5 | 0 | 0 | 0 |

Form bb-3. Road Erosion Worksheet

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|-------|-----------|----------|-------|----------|---------|--------------|------------|----------|----------|----------------------|----------|----------|------------|-----------|-----------------|-------------------|--------|-------|------|------|------|------|-------|
| _ | | | | | | | | | | | | | _ | | | | | | | | | | |
| EDe + | | (16) | | EDe | | 2 | 2 | 2.5 | 2.0 | 2 | 2 | 2 | | NG NG | (38) ER | Light | 19 | 6 | 10 | 19 | 48 | 48 | 9 |
| | + | (15) | Armor | Factor | | T | 1 | 1 | 1 | - | - | - | | GAMING | (23) ER | Heavy | 143 | 22 | 62 | 144 | 363 | 363 | 72 |
| | DITCH | (14) | Armor | X.X | | z | z | z | z | z | z | z | | | | | | | | | | | |
| | | (13) | Value | Œ | EB-0.05 | 2 | 2 | 2.5 | 2 | 2 | 2 | 2 | | | (28) Hazard | Rating H/M/L | | J | J | L | J | 1 | L |
| EFe + | | (12) | | BRe. | ٦ | 4.24 | œ | 1.8 | 5.0 | ∞ | ∞ | 80 | ■ ER | | (27) Overall | ER Rate Uacht | 7.6 | 2.0 | 9.6 | 5.4 | 20.0 | 13.7 | 2 |
| | OPE | (11) | Veg | Factor | | 0.53 | - | 0.18 | 0.63 | 1 | 1 | 1 | x ERd | RY | (36) | ERd | 0.3 | 0.1 | 0.3 | 0.3 | 0.5 | 0.5 | 0.1 |
| | FILLSLOPE | (01) | 88 | % Neg | | œ | 0 | 88 | 92 | 0 | 0 | 0 | | DELIVERY | (25) Direct | Entry %/100 | 0.33 | 0.1 | 0.33 | 0.33 | 0.5 | 0.5 | 0.1 |
| | | (6) | Value | BF | EB-0.20 | 8 | 8 | 10 | œ | ∞ . | 8 | 80 | | | (24) Buffer | Factor N = 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ECe + | | 8 | | ථු | | 8.48 | 10.08 | 7.4 | 8.5 | 16 | 16 | 10.08 | = ERe | | (23) | ERe | 23.12 | 20.22 | 29.2 | 16.4 | 40 | 27.4 | 20.22 |
| | HI D | 9 | Veg | Factor | | 0.53 | 0.63 | 0.37 | 0.53 | 1 | 1 | 0.63 | | ည | (22) | ETec | 8.4 | 0.14 | 17.5 | 0.8 | 14 | 1.4 | 0.14 |
| | COISCOPE | 9 | 8 | Veg | | Œ | 20 | 20 | 39 | 0 | 0 | 20 | | TRAFFIC | (21) Use | Factor | 1 | 0.01 | S | 0.1 | 1 | 0.1 | 0.01 |
| | | ଚ | Value | | EB V. | 16 | 16 | 20 | 16 | 16 | 16 | 16 | e = ETec) | | (20) Road | Use | ڻ ن | : | L | z | D | z | Ь |
| | | € | Basic | Erosion | Kate-EB | 5 | 40 | 50 | 40 | 40 | 40 | 40 | (ETe x Use | | (19) | ETe | 8.4 | 14 | 3.5 | 8.4 | 14 G | 14 N | 14 |
| 9 | | ල | Rock | Type | | Andesite | Andesite | Alluvium | Andesite | Andesite/ Granite | Andesite | Andesite | | SURFACING | (18) | Surface Factor | 9.0 | 1 | 0.2 | 9.0 | 1 | 1 | 1 |
| | | <u>ල</u> | Road | Age. | | >3 | >3 | >3 | >3 | >3 | >3 | >3 | | | (17) Value | ET EB*0.35 | 14 | 14 | 17.5 | 14 | 14 | 14 | 14 |
| | | Ξ | Road | Segment/ | 3110 | O9 | Put-to-bed | 79 | Nonuse | Bobcat Titicaca | | | ' | | | | | | | | | | |

TOLT RIVER WATERSHED ANALYSIS

SURFACE EROSION MODULE/ HILLSLOPES

by Nancy Sturhan, Soil Scientist DNR Forest Practices Division

The surface erosion module, hillslopes section addresses such hillslope erosion processes as rilling and gullying. Sheetwash erosion is rarely seen in forests, but could occur in areas of contiguous compaction and exposure of mineral soil.

METHODS

Because the eastern half (higher elevation) of the Tolt basin was under snow during the analysis period, different methods of analysis were possible for the western lowlands vs. the eastern highlands. Assessment of hillslope surface erosion for the eastern highlands relied heavily on remote methods such as analysis of aerial photography, topographic maps, and the Soil Erosion Potential GIS layer. Field visits were possible in the lower basin to verify information gleaned from photo and map analysis.

Because of the necessity of relying on remote analysis in the eastern highlands, map units there are drawn perhaps a bit more extensive than might be possible under thoroughly field-checked conditions. A few extreme surface erosion situations, such as dragging logs across a stream, are visible on aerial photos, but reliance on information on <u>potential</u> surface erosion was used to extend map units into areas where extreme situations had not occurred or are not visible, but more subtle surface erosion might be occurring.

Visits were made to many of the harvest areas in the lower basin. Of the 31 sections that had timber harvested in them in the past five years, harvest sites in 13 sections were visited. In addition, field forms were completed for sites where surface erosion was observed on the ground or suspected from aerial photos. Eighty percent of these sites were found to be unable to deliver sediment to the streams, primarily due to the topography.

Past logging techniques were deduced from 1965 1:40,000 aerial photos. At that time large contiguous areas had been logged in

the South Fork, the North Fork, and the lowlands. Logging extended to the creek. In some cases presence of a road on one side of the creek, with logging on both sides, may indicate yarding through the creek where full suspension was not likely. Current practices of leaving riparian zones for stream protection and yarding away from streams are all important improvements in logging techniques that can reduce the amount of surface erosion material reaching streams. Current logging practices in the Tolt basin have not covered as large contiguous areas as in the past. The table on page 7 shows that most recent logging has been on the lower erosion potential areas.

In general the amount of hillslope surface erosion that reaches the stream system is minor compared to the amount of fine material introduced from roads or debris events that introduce fines to the stream system. Hillslope sources of erosion tend to heal over time, where road surfaces will continue to provide fines to the system. Hillslope sources can be prevented or minimized by protecting the forest floor during harvest and site preparation. Protecting the forest floor near streams is the key to keeping hillslope erosion products out of the stream system.

SURFACE EROSION MAP UNITS General Information

Surface erosion map units were developed that reflect the likelihood of surface erosion products being delivered to the stream system. The Surface Erosion Potential (SEP) GIS layer, which combines soil properties and slope as criteria for High-Medium-Low ratings, was developed a number of years ago as a comparative rating system that attempts to separate the obviously low and high potential surface erosion areas from average areas. The surface erosion potential polygons were developed using a combination of slope and soil texture as criteria. affects the cohesiveness of soil as the finer clays help hold soil together, while sands do not hold themselves together well. For delivery and routing, coarse material tends not to travel as far as fine material. No deliverability of the erosion products was considered in the designation of the SEP rating system, and it should not be confused with the High-Moderate-Low Hazard ratings used in watershed analysis where deliverability is considered.

The actual hazard areas should be considered as occurring on the ground between the stream channel and a distance of 50 feet horizontal distance for Moderate, and 75 feet horizontal distance for High, from the stream. Horizontal distance is used so that the slope distance will be farther on steeper slopes. It is not

possible at the map scale used to accurately indicate the actual distance from the stream that should be considered to represent the hazard area. In the lowlands, the mapped locations were drawn thick enough to be able to display the appropriate hazard symbol. In the uplands the original surface erosion potential polygons are preserved, and the hazard area is that area within the mapped polygon that occurs within 50 feet horizontal distance of a Type 1-5 stream on Moderate Hazard or 75 feet on High.

PRESCRIPTION NOTES

Triggering Mechanism

All map units share some triggering mechanisms. Map units differ in the degree of susceptibility to the triggering mechanisms, and in the reasons for susceptibility. All map units are susceptible to soil disturbing activities that extend to the stream channel. Exposed mineral soil extending to the stream provides a direct route for surface erosion products to reach the stream. An example of this type of activity is where yarding scars extend to the stream channel.

The map unit that occurs in the upper river valleys on alpine glacial deposits is also susceptible to erosion by channelized flow that can result from such practices as installation of a culvert that is angled such as to direct flow against the banks of a channel, or blockage of a shallow drainage channel that overflows and cuts a new channel. Flow concentration can cause gullies to develop in this soil, as well. This map unit occurs on lower slopes that transmit a lot of water through the soil, and compaction or other soil disturbing activities are more likely to be delivered to the stream system where subsurface flows come to the surface.

The forest floor is the key in protecting soil from erosion. Where the forest floor remains intact, hillslope erosion does not occur. Where the forest floor is disturbed, erosion can occur. Where this disturbance leads to the stream, erosion products can be introduced to the stream system, the finer soil materials may travel far, coarser ones tend to deposit nearer the site where they originated.

Practices that help protect these surface erosion sites are those that preserve the herbaceous vegetation, shrubs, and forest floor intact near streams. Full suspension of logs is a practice that virtually eliminates disturbance of the forest floor during logging. One end suspension of logs and yarding away from streams can help minimize the introduction of surface erosion material to streams.

SURFACE EROSION MAP UNIT DESCRIPTIONS

There are five Surface Erosion Map Units identified for the Tolt watershed. The map units are separated into those of the lower basin in the western half of the watershed which is an area of low relief, and the upper basin in the eastern half of the watershed which is an area of steeper, more dissected terrain.

| HAZARD RATING | GENERAL LOCATION |
|--------------------------|--|
| | |
| | |
| HIGH MODERATE | steep terrace risers adjacent to streams medium erosion potential next to streams |
| | |
| HIGH MODERATE HIGH | steep slopes of upper watershed medium erosion potential on steep slopes alpine glacial deposits in upper river, both forks, adjacent to streams |
| | HIGH MODERATE HIGH MODERATE |

SURFACE EROSION MAP UNIT 1

Areas mapped SE1 occur on the steep terrace risers in the lower basin. Steep slopes on the glacial outwash deposits are susceptible to erosion from soil disturbance. Where these slopes occur adjacent to the stream system, they are mapped as SE1. Where the access to the stream system is interrupted by the lower terrace, erosion products are assumed to not be delivered to the stream system. Where streams are deeply incised into the glacial outwash deposit, sideslope tend to be especially unstable and susceptible to surface erosion.

Triggering mechanism: Disturbance of soil on the steep slopes adjacent to the stream system may cause soil material to deposit in the stream. Where continuous soil disturbance extends to the stream (ie yarding scars, road fill, gullies, etc.), delivery of erosion products is certain. Excessive soil disturbance on the hillslopes makes delivery to the stream system more likely because more material is dislodged and available for movement downslope. Where there is continuous vegetation cover, and/or the intact forest floor, adjacent to the stream, surface erosion products may not be delivered to the stream at SE1 sites.

SURFACE EROSION MAP UNIT 2

Areas mapped as SE2 occur on the soils less likely to erode than SE1, but where these soils occur adjacent to streams, there is a moderate hazard for delivery of soil material to the stream. This map unit occurs on the lower relief of the western half of the basin. SE2 mapped areas usually occurs on less steep terrace risers and other slopes where the streams tend to cut into the glacial deposits as they travel down the moderately steep pitches. Triggering mechanisms are the same as in SE1.

SURFACE EROSION MAP UNIT 3

Areas mapped as SE3 occur on steep slopes adjacent to the stream system in the upper basin. Many of these areas are also susceptible to shallow rapid mass wasting. The more highly dissected terrain has many occurrences of SE3 and SE4. Most streams in the upper watershed are partly or entirely in one of these map units. Triggering mechanisms are essentially the same as SE1.

SURFACE EROSION MAP UNIT 4

SE4 units are less susceptible to erosion than SE3 due to slightly gentler slopes or more cohesive soil structure. Triggering mechanisms are essentially the same as SE1.

SURFACE EROSION MAP UNIT 5

Areas indicated as SE5 occur in the upper river valleys of both the North and South Forks of the Tolt River. These deposits generally lie at low relief, but are easily eroded where they occur on steep slopes. Where streams cut through this material, the sideslopes may be steepened, and there is access to the stream system for erosion products

Triggering mechanisms in addition to those for SE1 include directing flow of water towards this soil by blocking or deflecting the flow of a channel.

CONFIDENCE

Confidence in the hillslope surface erosion map units for the western lowlands can be considered high. Characteristics of the topography played a strong role in limiting the deliverability of surface erosion products to streams in most cases. The sites where hillslope surface erosion products could reach a stream are

delineated with high certainty. Geology interpretations, map and photo analysis, and field visits were in agreement, confirming the calls on hazard areas in the western lowlands.

Confidence in the hillslope surface erosion map units for the eastern highlands is somewhat lower than that for the lowlands. While geology, soil maps, and photo interpretation are in agreement to support the map units, field visits to the eastern highlands were limited. Because the actual map units are tied to proximity to the streams, the units likely capture the vulnerable areas. Field visits would locate areas where topographic or vegetative buffers may be acting to limit delivery. Also, field visits could locate areas where gullies not visible on photos actually extend some distance from the stream. Gullies that reach the stream system can be considered as part of the stream for delivery purposes, and can be protected from disturbance along the edges, limiting introduction of more surface erosion products into the stream system.

Certainty of the High vs Moderate calls is low between map units 3 and 4, relying on the SEP for that distinction. That difference may not be important to the prescription team, but if it is important, further field work would be required to distinguish the High from Moderate areas. If the team chooses to treat the Moderates as Highs, particularly in areas where the rule call is prevent or avoid, then further distinction would not be needed.

ADDITIONAL BACKGROUND MATERIAL

Soils have been classed by the soil survey as "fine", "medium", and "coarse" texture. A map has been provided showing the locations of these soils. To have significant amounts of clay, soils either develop from clay-rich parent material, or develop in place for a long period of time to produce clays. About 2% of the entire Tolt basin has the "fine" soils, none in the South Fork. Some of the coarse soils are described as having "pockets of volcanic ash" which would be a fine material, but apparently About 48% of the entire Tolt basin is in is not extensive. medium texture soils, and about 49% in coarse texture soils. The coarse soils and medium texture soils tend to be gravelly sandy loams(10-20%clay) or gravelly loamy sands(8-28%clay). coarse soils tend to have >50 % rocks, while the medium texture soils in the Tolt tend to have 20-50% rock. The fine soils are silty clay loams. The fine soils in the Tolt developed from lakebed deposits, a clay rich parent material. The coarse and medium texture soils in the Tolt are too young to have developed much clay from their coarser parent materials. On the steeper slopes the soils remain perpetually young due to natural erosion processes.

TOLT - RECENT HARVEST

Area harvested in the past 5 years (1988-1992)

Harvest per surface erosion potential class

| LOW | 900 Ac. | 54% |
|--------|---------|-----|
| MEDIUM | 625 Ac. | 37% |
| HIGH | 155 Ac. | 98 |

Area of the TOLT Basin per surface erosion class

| LOWLAND | LOW | 60% |
|------------|--------|-----|
| | MEDIUM | 35% |
| | HIGH | 5% |
| HIGHLAND | LOW | 20% |
| | MEDIUM | 55% |
| | HIGH | 25% |
| | | |
| TOLT BASIN | LOW | 40% |
| | MEDIUM | 45% |
| | HIGH | 15% |
| | | |

Most harvest in recent years has been on soils least vulnerable to surface erosion.